Inspector's Record

MUD ROAD, HAMBDEN

CEDAR ROAD, CHESTER

DIETZGEN

TRADE MARK

ENGINEERS'

LEVEL BOOK

No. 410

64

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning

Roadway 16 feet wide. Side Slopes 1 on 1.

For Single Track Embankment.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

64

Cedar Road - No. 98 - Sec. B

Align. - pg 32-56, 78-92

X-Sec. - pg. 58-76, 93-116

Slope Stakes - pg. 117-146

Cedar Road - No 98 Sec C

Align Pg 147-153

Pages 1 to 27 were used as inspector's record, Mud Rd., Hamden.

Cedar Road W. of Chittenden Road in Chester

Road Records Book B. - P. 342

Statute width Mar. 3, 1828. 60 ft

petition signed by Aaron C Jacobs and others was presented to the Board. Oct. 21, 1827

Survey of a Road beginning at the northwest corner of lot No. 1 in part 3 in the Township of Chester thence running N. 87° E on the north line of lots No. 1, 2, 3, 4, 5, & 6. 2 miles 55 chains 17 links to the center of the Chittenden road in said Chester

Chester Dec 14th 1827

Attest George E. White
Surveyor

At a meeting of the Board of Commissioners aforesaid held at Chardon on the third day of March the year one thousand eight hundred twenty eight the committee aforesaid made their report as follows;

"Agreably to the directions of the above order the undesigned committee have proceeded to discarge the duties assigned them and have caused the above described Road to be laid agreably to the survey and protraction of George E White and would report that in our opinion said road aught to be established & opened. Silas Tanener, Eber Norton, Sibens Norton } committee

Which said report having been publickly and audibly read on two different days of the meeting last aforesaid and the same being duly examined, considered and fully undestood by the Board and they being satisfied that said road would be of utility to the publick.

It was thereupon ordered that the same be established and henceforth taken deemed and considered as public highway pursuant to the Statute in such case made and provided, and that the same be opened and Recorded

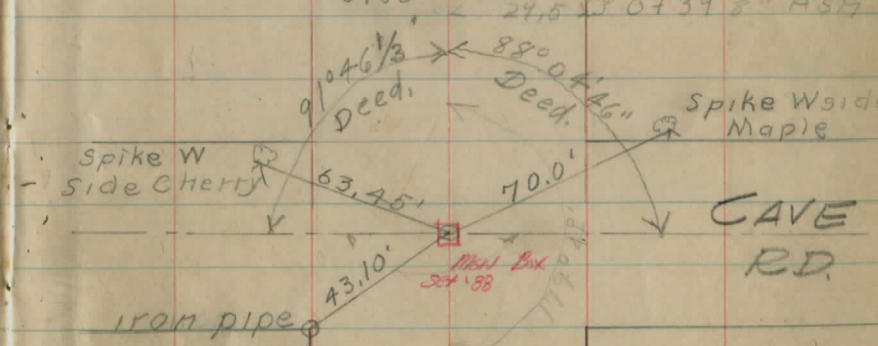
attest Ralph Cowles
clerk to Commissioners

Cedar Road,

0+00 Iron Pipe, ℄ N.+S. Rd., (Cave Road)

1+50 × 25 ⊗ ↗
< 22.5 × 1+50
< 29 × 1+45 10" Apple
< 29.5 × 1+39 6" Apple
< 28 × 1+28 12" Apple
< 28.5 × 1+20 12" Cherry

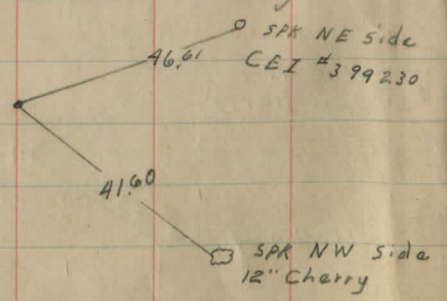
10" Apple 1+10 < 19.5 >
20" Beech 1+03 < 23.5 >
12" Maple 1+02 < 17.5 >
1+00 × 25' ⊗
18" Cherry 0+75 < 28 >
6" Maple 0+66 < 27 >
22" Twin Cherry 0+63 < 25 >
8" Maple 0+40 < 22.5 × 28.5 × 0+70 20" Cherry
8" Cherry 0+54 < 22.5 >
8" Maple 0+50 < 22. × 30.5 × 0+49 15" Cherry
0+50 × 25'
< 24.5 × 0+39 8" Ash



4+45 Spike Δ=0°00'

~~3+00~~ Spike Δ=0°00'

2+98.10 SPK Δ=0°00' May 1957



< 18 × 5+99 6" Apple
< 16 × 5+59 3" Hickory
< 15 × 5+56 3" Apple
5+12
⊗ 25' × 5+50
< 8' 5+40
chicken house
39' × 5+04 20" Apple
50' 5+08
⊗ 25' × 5+00
15" Ash 4+85 ⊗ 31.5 >
⊗ 25' × 4+00
15" Ash 4+40 ⊗ 27.5 >
15" Beech 4+37 ⊗ 28.5 >
12" Ash 4+25 ⊗ 34.5 >
39' ⊗ 36" Apple 4+65
⊗ 25' × 4+00
⊗ 25' × 3+50
24" Maple 3+50 ⊗ 33 >
< 17 × 3+48 8" Chestnut
12" Cherry 3+35 ⊗ 24 >
< 10 × 3+47
15" Cherry 3+10 ⊗ 21.5 >
Spike 3+15
14" Ash 3+02 ⊗ 14 >
1' ⊗ 25 × 3+00
8" Elm 2+94 ⊗ 22 >
18" Cherry 2+90 ⊗ 19 >
15" Cherry 2+84 ⊗ 19.5 > × 30 > 2+47 10" W. Cherry
12" Cherry 2+63 ⊗ 19 >
12" Cherry 2+57 < 24 × 30 > ⊗ 2+44 15" W. Cherry
⊗ 25 × 2+50
12" W. Cherry 2+45 ⊗ 20 > 28 > ⊗ 2+35 12" Cherry
18" W. Cherry 2+20 ⊗ 17" × 28.5 ⊗ 2+14 10" Ash
2+00 × 25' ⊗

Fair 60°

D. Parks

Stopped march 10 1930 F. Grau.

⊗ 25' × 8+50

8" Beech 8+48 ⊗ 40.5 >

10" Ash 8+40 ⊗ 33 >

8" W cherry 8+48 ⊗ 29 > < 13 ⊗ 8+40 Dead apple

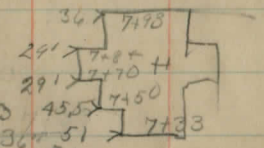
8" Ash 8+30 ⊗ 40 >

10" Maple 8+12 ⊗ 31 > 8+62 Drive

15" Ash 8+07 ⊗ 39 >

6" Ash 8+00 ⊗ 36 25' × 8+00

< 19 ⊗ 7+97 30" Elm



⊗ 25 × 7+50

< 20,5 ⊗

< 7 > 7+41

< 12 > 7+20 Beech

⊗ 25' × 7+00

100 > 7+00

Lilac Bush

< 28 ⊗ 6+91

Japanese Quince

4" Ash 6+87 ⊗ 32.5 < 3.5 ⊗ 6+89 Beech

6" Ash 6+81 ⊗ 37 >

4" Ash 6+75 ⊗ 31 >

15" Ash 6+63 ⊗ 38 25' × 6+50

8" Ash 6+37 ⊗ 33,5 × 34,5 ⊗ 6+50 10" Apple

< 2' ⊗ 6+76 4" Maple

12" Butternut 6+21 ⊗ 40 >

< 36,5 ⊗ 6+16 21" Apple

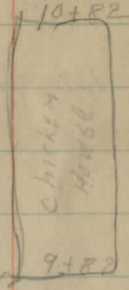
< 23'

⊗ 25' × 6+00

100' 7+01

9+35 spike Δ=0°00'

8" Elm 12+82 30.5 >
20" Maple 12+72 45 >
25' × 12+50
20" Apple 12+42 45 >
< 4 > 24
< 3.5 >
24 Wchm 12+06 4.5 >
25' × 12+00
< 2 > 4" Bass Wood 11+74
11+75 18" Elm 45 >
11+66 20" cherry 45 >
25 × 11+50 24 > 11+64 20" Appl
28.5 > 11+36 Basswood 6"
11+15 18" Maple 45 >
11+10 25' 14 > 11+18 Hickory
< 4.5 > 10+90
11+96 30" Ash 40' >
14 > 10+65 18" Apple
25' × 10+50
< 13.5 > 10+35 12" Apple
9+85 30" Elm 40' >
< 14 > 15" Apple
< 14 > 9+79
9+50 10" Ash < 38' > 9+50 25' Iron Pipe
9+45 8" Ash < 36' >
9+11 < 15
9+03 8" Ash < 34 >
25' × 9+11



9769 House 9+47

10.6 X 4'

14+75.75 Concrete Slab top 1'X4' Wing Wall

14+51.2 Spike Δ = 0°00'

16+59 6" Sycamore ℄ 28 >

14+62 15" cherry ℄ 31' >

℄ 25' x 16+00

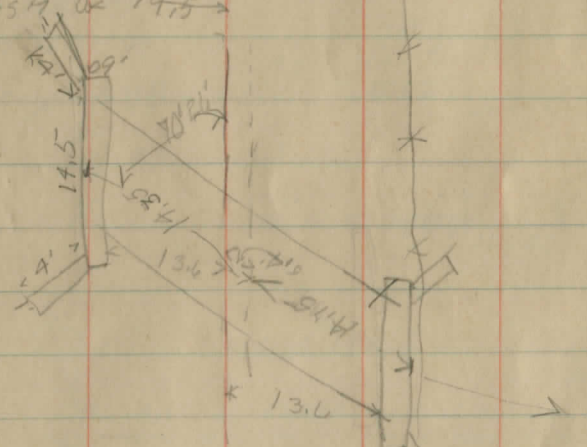
15+92 10" cherry ℄ 35 >

15+52 20" cherry ℄ 35 >

℄ 06 ✓ 15+15

15+00 x 25 ℄

14+93 12" Ash ℄ 19.5 >



14+54 8" Walnut ℄ 20.5 >

35 ℄ 17.5 ℄ 12" Walnut

℄ 18 ℄ 17+31

36" Willow

℄ 25' x 14+00

13+67

13+60 15" Cherry ℄ 40 >

13+52 on ℄

℄ 11.5 > 13+26 4" Elm

℄ 25' x 13+00

41

42

22785 10" cherry @ < 38 >
22781 10" cherry @ < 38 >

@ 25 x 22700

@ 25 x 21700

21700 cherry @ < 38 >

20792

20467 8" cherry < 40 >
21+36 12" cherry < 38 > x 20 10" Maple cc
20+37
20+12 x x < 33 >

@ 25 x 20700

< 10.5 19+15

@ 25 x 19+00

18+94 8" cherry < 35 >

15" Cherry < 35 >

@ 25 x 18+00

< 12.5 > x x 17+73

< 08 > 17+55

@ 25 x 17+00

D. Parks
F. Gray
R. Goodrich
C. Trane

Cold Snow

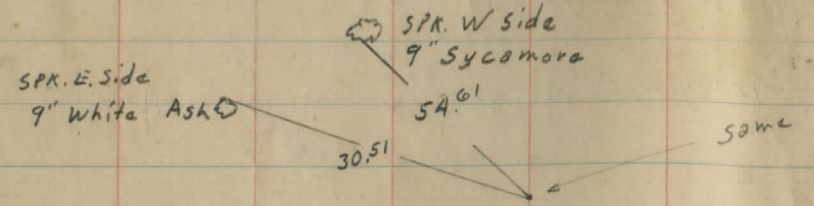
" stoped March 11. 1930

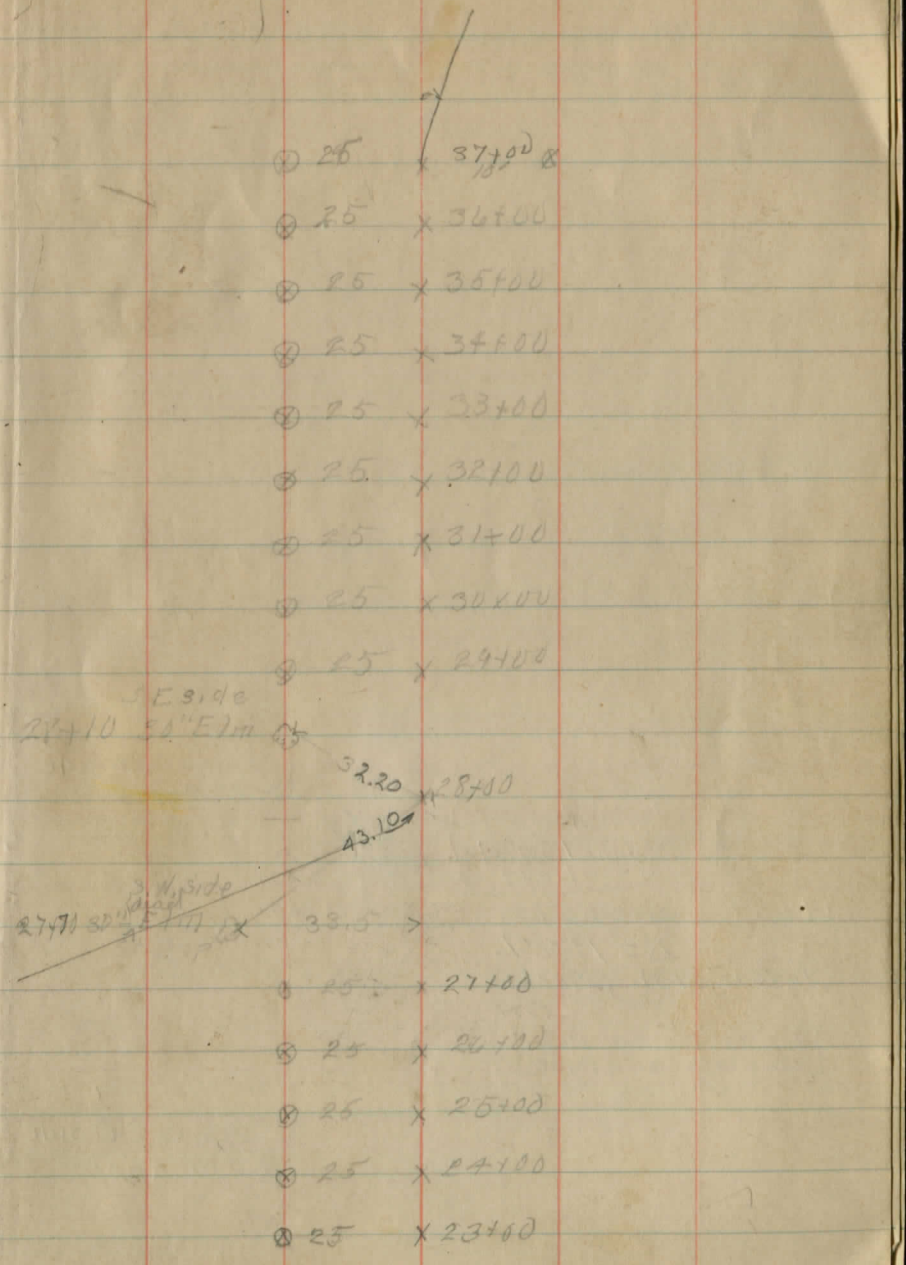
37+00 ~~Spike~~ ~~Δ = 0°07' R.~~

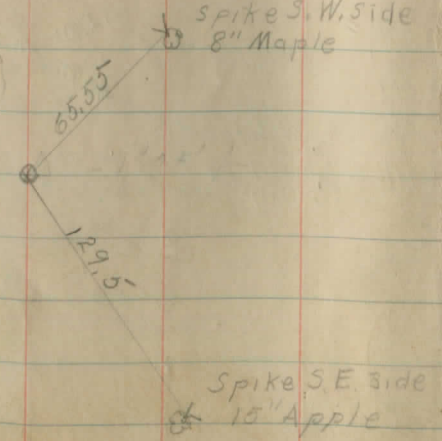
Bolt Δ = 0°00'

Moved point South 0.40' to be on straight Line between 28+00 and 39+65.5
June 15, 1931, Marks, Post.

28+00 Spike Δ = 0°00'







39+65.5 ~~A=10°05'L~~
Δ = 1°00'L
June 15, 1931, Markst
Pist
[Corrected on Map
June 15th '31 - Post]

20 > 41+92 10" Beech
18 > 41+86 15" Beech
> 41+89 20" Wcherry
> 41+55 10 Wcherry
10 > 41+32
25 x 41+00
15 > 40+78 2" Ash
10 > 40+49 Ash 4"
16 > 41+28 11" Maple
25 41+10
25 x
27
25
37 > 38+41
37 > 38+29
37 > 38+13
25
38+00
30'
37+60

Cold Wind D. Marks, R. Goodrich, C. Rand

Stopped March 13 1930

June 15, 1931, Marks, Post

44+65.75 Δ=0°30'30" Lt.

52.70 → Spike N side 12" Elm

121.65 → Spike E. side 14" Elm

30° appk 48+87 ∠ 25 × 48+83 W cherry

∠ 21 × 48+43.8 Maple

25 × 48+00

47+91

∠ 23.5 × 47+88 W cherry

16" Appl 47+67 ∠ 13 ×

∠ 24 × 47+38 18" Maple

∠ 13 / 25 ×

∠ 22 × 46+95 12" Maple

∠ 24 × 46+72 15" Maple

25 × 46+00

∠ 24.5 × 45+72 15" Elm

25 × 45+00

∠ 24.5 × 44+65.75

∠ 23.5 × 44+07 20" cherry

25 × 44+00

∠ 22.5 × 43+96 10" cherry

∠ 23 × 43+46 15" Elm

∠ 21 × 43+23 6" Elm

∠ 22.5 × 43+21 10" Elm

25 × 43+00

25 × 42+00

50+70,5 4.5 X 4.5 Stone Box Culvert
Fair

23" Cherry 51+90 < 23 >
20" Maple 52+35 < 22 >
30" Elm 52+11 < 23 >
12" Butternut 52+06 < 24 >
< 25 > 52+00
< 21 > 52+55 15" Maple
< 35 > 52+12 40" Beech
11" Maple 51+62 < 24 >
10" Maple 51+37 < 16,5 >
15" Ash 51+34 < 24 >
15" Ash 51+14,5 < 7 >
< 20 > 51+32 10" Ash
< 25 > 50+00
8" cherry 50+80 < 13 >
< 18 > 50+82 8" cherry
1.7
4.6 x 11.7
10" Hickory 50+47 < 07 >
12" Maple 50+35 < 04 >
10" Wchen 50+27 < 06 >
50+08 < 24,5 >
< 25 > 50+01
15" Maple 49+81 < 21 >
24" Maple 49+78 < 14 >
< 25 > 49+78 8" Maple
< 22 > 49+31 30" Maple
< 25 > 49+01

#75770

56+92 L19 28 56+67

24 56+60

24 56+16 15" Maple

#75771

SPK CE1 #0 399069 CE1 25 56 Manhole

55+38 18 17 55+61

37 87 16 55+10

26 55+01 12" Maple

55+05 88 P.O.T. 25 55+00 25.56 SPK E. Side 15" Maple

26 54+88 36" Elm

54+85

24 54+11 12" Maple

25 54+00

CE1 Bell 19

#75772 53+80 18

24 53+60 Mahogany

20" Maple 53+54 21

150 53+60 Garage 53+40

53+49

53+35

100' H

53+00 53+08

12" ash 53+39 25

36" Maple 52+10 40

0025

15" Ash 52+84 22

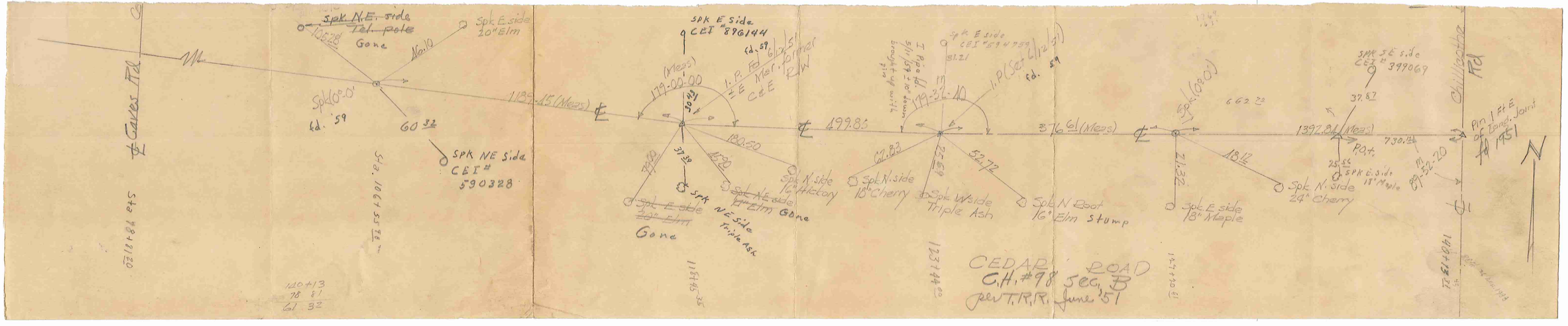
18" Mahogany 52+72 22

16" Ash 52+71 22

12" Cherry 52+69 22

8" Maple 52+66 22

32 52+61


Gaves Rd
Spk NE. side Tel. pole Gone
10628
No. 10
Spk E side 20" Elm
Spk 10°-0' Ed. '59
1183.45 (Meas)
60 32
SPK NE Side CEI # 590328
Sta 1067+55.52
Sta 984+20
140+13
78 81
61 32
SPK E Side CEI "896144
Ed. '59
(Meas) 179-00-00
I.P. Fd 6 1/2" I.E. Mer. former R/W
C & E
Spk
37.39
180.50
499.85
Spk N. side 16" Hickory
Spk E side 20" Elm Gone
Spk NE side 14" Elm Gone
SPK NE Side Triple Ash
1164.35
Spk E side CEI "594739
Ed. '59
I.P. (Set 6 1/2" I.E.)
179-32-10
Spk N. side 18" Cherry
Spk W side Triple Ash
Spk N Root 16" Elm stump
1231.44
CEDAR ROAD
C.H. #98 Sec. B
Jen T.R.R. June '51
376.61 (Meas)
Spk (090°)
662.22
SPK E Side CEI # 399069
37.87
1397.84 (Meas)
Pt.
730.12
25.55
SPK E side 18" Maple
Spk N. Side 24" Cherry
87-52-20
Chillicothe Rd
Pin 1 Ft E of Conc. Joint
1951
1441.90

53

58+00 3 X 3,5 Stone Box good.

54

23 ⌀
23 ⌀
23 ⌀ 3" Maple
25' apart

#552250 ⌀ 60+96 <SEI 23 19> 61+00

61+02
100
60+86

⌀ 23 61+00
60+90
Bell Tel. 14 cherry
60+73
< 15
23
< 10 > 60+65 x P⊥P
< 23 > ⌀ 60+55 8" catalpa

⌀ 25 x 60+00

8" Maple 59+53 < 13 >

#552251 59+44 <SEI 19 >

59+39
H
100
57+17

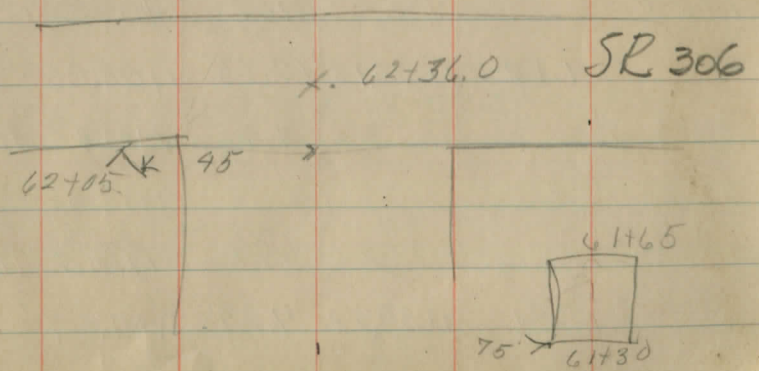
⌀ 25 x 59+06
< 15 > 58+85
58+76
58+67 Garage
110
58+64

58+52
< 21 > 18" Maple

#75769 58+37 <SEI 19 >

⌀ 25 x 58+06
1.6
12.9
8.5
11 x 15.0
8.3
12.9

< 28 > ⌀ 57+25 10" Ash
BEI
< 18 > 57+23
⌀ 25 x 57+04


62+36.0
SR 306
62+05
45
61+65
75
61+30

B.M.	5.99	1136.22		1130.23
62+36.0				
	8.80	1145.01	0.01	1136.21
62+36.0			6.5	1138.5
+25			4.5	1140.5
+63+00			4.2	1140.8
+63+50			3.8	1141.2
+64+00			2.9	1142.1
+64+50			2.0	1143.0
62+00			6.6	1138.4
61+00			10.2	1134.8
	1.12	1135.18	10.95	1134.06
60+00			4.4	1130.8
59+00			6.7	1128.5
	2.91	1130.80	7.29	1127.89

& Chillicothe Rd

Stupl E. root 24" Maple. 30'lt sta 20+10

1131.9 / 4.3 / 160 — 1128.4 / 7.8 / 250

1144.1 / 0.9 / 200 — 1141.4 / 3.6 / 200 — 1140.2 / 4.8 / 50 — 1139.8 / 5.2 — 1138.5 / 6.5 / 30 — 1137.0 / 8.0 / 30 — 1136.7 / 8.3 / 50

5.1 / 30 — 5.8 / 23.5 — 7.7 / 22.5 — 7.2 / 17 — 6.6 / — — 8.7 / 17 — 7.8 / 30

7.8 / 30 — 8.8 / 13.5 — 11.2 / 8.5 — 10.2 / — — 10.7 / 12 — 9.7 / 30

2.6 / 30 — 3.9 / 10 — 6.8 / 7 — 4.9 / 3.5 — 4.1 / — — 4.8 / 7 — 5.9 / 11.5 — 2.7 / 25 — 2.4 / 30

9.9 / 30 — 7.6 / 10 — 8.5 / 7 — 7.4 / 5.5 — 6.7 / — — 8.5 / 11 — 7.4 / 30

		1130,88		
58+00			4.5	1126.3
58+00 earth work Calculations only				
57+00			3,9	1126.9
	8,43	1136,17	3,06	1127,74
56+00			5,9	1130,3
55			5,0	1131,2
B, M			4,74	1131,43
54			9,1	1127,1
	0,67	1126,59	10,25	1125,92
53			6,6	1120.0
52			12,2	1114.4
	1,93	1116,66	11,86	1114,73
51			4,5	1112,2

1126.3 1124.3 1121.3 1124.8 1127.9 1126.3 1126.3 1125.6 1127.4 1124.3 1120.9 1120.1 1119.5 1117.4 1116.3

4.5/100 6.5/30 7.5/11 6.0 2.9 4.5/7.4 4.5/2 5.2/13.4 3.7 6.5/15 9.9 10.1/50 11.3/100 13.4/200 14.5/300

5.6/30 6.2/15 7.1/15 8.4/30

1.5/30 4.3/3.5 3.9/2 3.5/3 4.6/11.5 2.2/20.5 3.4/30

4.3/30 5.6/5 7.0/3 5.9/2 5.2/5 6.0/10 6.8/13 4.1/17.5 6.1/30

4.2/30 5.1/4.5 5.6/3 5.0/2 4.5/5 5.7/13 5.4/15 5.5/30

N. E Root 36" Beech 60' Rt Sta. 54+60

5.4/30 7.8/7 10.0/3 9.1/2 8.6/4.5 9.5/11 7.3/17.5 6.1/20 6.1/30

2.6/30 2.6/16.5 6.5/8 7.7/6.5 7.1/4.5 6.6/2 7.4/7.5 2.1/17 0.3/25 0.2/30

15.2/30 12.7/6.5 13.2/4.5 12.2/2 12.0/3 13.3/11 15.0/30

7.3/30 5.7/6 4.5/3 4.5/2 4.4/3 4.8/10 5.4/11.5 8.6/30

	1116.66		
50+70,5		4.8	1111.9
50		3.8	1112.9
	10.54 / 126.70	0.50	1116.16
49		10.5	1116.2
48		3.5	1123.2
47+75		2.4	1124.3
B.M.		5.40	1121.30

Clear Cold. Windy 45° Temp.

Stopped Mar 14 1930

D. Parks, R. Goodrich, C. Ramey

1110.2 1109.2 1108.3 1106.1 1109.7 1112.4 1111.7 1111.9 1112.1 1112.1 1110.1 1106.1 1106.1 1105.8 1105.4 1104.6 1104.3 1102.4

6.5/150 7.5/100 8.7/50 10.6/50 7.0 4.3/4.6 5.0/8.2 4.8/2 4.6/11.3 4.6 6.6/12.7 10.6/50 10.6/100 10.9/200 11.3/300 12.1/400 12.4/500 19.1

4.2/30 4.6/10 3.9/7 3.8/2 3.4/4.5 4.4/10.5 4.0/11.7 4.0/30

3.9/30 3.7/11.5 10.8/2.5 10.5/2 10.3/3.5 10.9/8.5 4.7/15 4.7/30

0.7/30 1.7/10 4.3/2.5 3.5/2 2.9/5.5 4.2/12 2.6/15 2.6/30

0.5/30 1.3/9 3.1/7 2.7/2 2.1/5 3.3/12 2.0/13.5 2.0/30

N.W. Root 15" Maple 50 Rt. Sta. 48+30

B.M.	6.26	1127.56		1121.30
47			5.8	1121.9
46			7.6	1120.1
45			8.5	1119.2
44			10.0	1117.7
	3.62	1119.26	11.92	1115.64
43			3.4	1115.9
42			4.6	1114.7
41			6.7	1112.6
40			7.7	1111.6
	4.94	1116.87	7.33	1111.93
39+37			4.5	1112.4

N.W. Root 15" Maple 50' Rt. Sta. 48+30

3.4 / 30	3.5 / 17	3.3 / 12	5.0 / 5	6.7 / 3	5.8 / 2	5.1 / 6	6.0 / 12	6.8 / 17	4.3 / 14	4.2 / 30
7.7 / 30	7.8 / 8	8.8 / 5	7.9 / 2.5	7.6 / 2	7.2 / 7.5	7.9 / 10.5	8.4 / 13	8.1 / 15	8.1 / 30	
8.5 / 30	8.1 / 7	9.9 / 5	9.2 / 3	8.5 / 2	8.2 / 4	9.0 / 10.5	9.5 / 12.5	8.8 / 14	8.8 / 30	
8.6 / 30	9.3 / 25	10.4 / 10.5	12.0 / 7.5	10.9 / 5	10.0 / 2	11.1 / 7.5	12.1 / 7.5	10.7 / 11	10.2 / 30	
4.4 / 30	4.4 / 11.5	4.8 / 10.5	5.0 / 8.5	3.4 / 2	4.2 / 6.5	5.1 / 8.5	4.5 / 10	4.5 / 30		
4.7 / 30	4.7 / 19.5	6.5 / 11.5	5.4 / 9.	4.6 / 2	5.4 / 5.5	6.5 / 8	5.3 / 9.5	3.8 / 22	3.8 / 30	
6.0 / 30	6.6 / 14	7.6 / 12	7.0 / 9	6.7 / 2	7.2 / 4.5	7.9 / 6	7.9 / 7.5	6.1 / 11.5	6.1 / 30	
8.1 / 30	8.1 / 12.5	8.7 / 11	8.3 / 7	7.7 / 2	1111.6 8.8 / 5.5	8.2 / 7.5	7.9 / 17	8.8 / 30		
4.8 / 200	5.0 / 150	5.4 / 100	5.5 / 50	5.2 / 30	4.5 / 4	5.7 / 30	5.9 / 50	5.9 / 100	6.3 / 150	6.4 / 200

		1116,87		
39			5,7	1111,2
38			1,6	1112,3
	2,41	1117,86	1,42	1113,45
37			2,4	1115,5
36			4,5	1113,4
35			8,0	1109,9
34			10,4	1107,5
	5,47	1111,78	11,55	1106,31
33			5,5	1106,3
32			6,3	1105,5
31			6,6	1105,2
30			5,7	1106,1

1111,2

7,0	7,0	6,2	5,7	6,0	6,5	6,8	
30	11	7	2	8	10	30	
3,8	4,2	3,7	4,7	5,2	4,6	4,2	5,5	4,4	4,7
30	28	25	5,5	4	2	3	10	14	30
1,6	1,8	2,1	3,0	2,4	1,9	3,4	2,4	2,3	
30	25	6	4	2	3,5	11	12,5	30	
3,2	2,8	3,8	5,5	4,5	6,3	3,7	3,5		
30	20	10,5	7,5	2	9	11	30		
7,3	7,9	9,8	8,8	8,0	9,7	7,1	6,5		
30	11	10	7	2	8	11	30		
10,5	10,5	10,7	11,4	10,4	11,6	11,4	10,9	10,4	
30	20	9	7	2	9	12,5	13	30	
7,2	7,2	6,5	6,8	5,5	6,3	6,8	6,5	6,6	
30	12	9	7	2	7	9	11	30	
6,7	7,4	7,0	7,6	6,9	6,3	7,0	7,7	7,1	6,7
30	10	8	6,5	4	2	10	12	13	30

1105,2

7,6	7,6	8,0	7,4	6,6	7,1	7,7	7,1	7,4
30	8	7	6	2	10	12	13,5	30
6,3	6,3	7,0	6,3	5,7	6,3	7,0	7,0	5,8	5,6
30	10	8,5	6	2	7	8	10	12	30

	+		−	
		1111.78		
29			5.3	1106.5
B.M.				
28			5.9	1105.9
B.M.	2.05	1109.30	4.53	1107.25
27+30			3.7	1105.6
27			5.5	1103.8
26			9.4	1099.9
	2.76	1102.95	9.61	1099.69
25			3.9	1098.6
24			4.9	1097.6
23			7.6	1094.9
22			9.9	1092.8
	3.83	1096.19	10.09	1092.36
21			4.9	1091.3

4.6 6.5 6.0 6.4 5.3 6.0 6.7 6.0 5.8
30 14 12.5 9.5 E 7 7.5 9 30

7.2 6.5 6.7 6.4 5.9 6.8 6.3 6.0
30 12.5 11.5 9.5 E 6 7 30

R.P. Spike S.W. side dead Elm 33.5 Lt, Sta 27+72

2.7 2.5 4.9 4.1 3.7 4.4 5.5 3.2 2.8
30 14 11 8.5 E 4 6.5 9 30

2.8 4.1 6.2 5.5 7.9 5.5 4.4 4.6 3.6
30 16.5 12.5 10 5 E 3.5 6 30

7.3 8.0 9.0 7.8 8.2 9.7 7.9 7.5
30 17 14.5 8 4 E 2 30

3.2 3.2 3.7 3.3 2.6 3.9 3.9 3.7 3.9 3.9
30 16.5 15 13.5 8 4 E 1 5 30

4.8 4.2 3.9 5.2 4.5 4.1 4.7 4.7 5.0 5.7 5.3 4.8
30 21.5 17.5 14.5 13.5 6.5 E 2 6 7 10.5 30.0

6.8 7.2 8.7 7.6 6.8 7.6 4.8 8.8 7.7 7.7 6.4 4.6
30 17 16 13.5 7 E 1 2 3.5 3.5 9 30

10.1 10.2 10.5 9.7 8.8 9.4 10.4 9.3 8.5
30 18 17 15 9 E 1 2 30

5.2 4.8 6.1 5.2 4.6 4.9 4.3 6.0 5.1 3.7
30 20.5 19 16.5 10 E 3.5 4.5 5. 30

		1096.19		
20			9.6	1086.6
19+50			10.5	1086.7
	3.89	1088.40	11.68	1084.51
19			5.9	1082.5
18			8.1	1080.3
17			9.8	1078.6
	5.44	1083.95	9.89	1078.51
16			6.4	1077.6
15			5.9	1078.1
14+75.75			5.0	1079.0
14			4.4	1079.6
	8.24	1090.18	2.01	1081.94
B.M			2.66	1087.52

Rain stopped March 17, 1930
P. Parks R. Goodrich C. Rand.

6.6 6.5 7.6 9.7 8.7 7.7 7.9 9.6 9.6 8.5 7.4 7.4 5.2 2.8
30 28 25 19.5 17 11 6 3 2 2 4.5 5.5 9.5 30

7.1 8.5 10.0 11.7 10.5 9.9 10.5 12.3 12.3 10.5 10.5 8.4 8.4 5.9 4.1
30 26 21 19.5 16.5 16.5 7 2.5 1 2 2 3.5 5 11 30

3.7 4.4 6.2 4.7 4.0 5.1 5.9 5.9 4.5 4.5 2.2 1.3 0.3
30 22 20.5 18.5 11 3.5 2 2 0.5 3.5 7 11.5 30

7.6 7.1 8.3 7.7 6.9 7.3 8.1 8.1 7.3 7.3 6.1 5.4
30 21.5 19.5 17.5 11 5 3 2 0.5 3.5 8.5 30

9.6 9.6 10.1 8.8 8.5 8.6 9.8 9.2 9.4
30 20.5 18.5 12 9.6 5.5 2 2.5 30

6.3 6.1 7.0 6.3 5.7 6.4 6.8 5.6 5.8
30 19.5 17.5 14 8.5 2 1 3 30

9.5 6.0 5.4 5.6 5.2 5.9 5.9 7.3 7.3 6.3 4.7
26 22 19.5 13 6.5 2 2 3 6 7 30

1074.8 1074.7 1074.4 1077.0 1078.0 1080.3 1079.0 1079.0 1078.9 1080.4 1078.0 1074.3 1074.6 1074.5 1074.5 1074.2 1073.2
9.2 9.3 9.6 10.0 6.0 3.7 5.0 5.0 5.1 3.6 6.0 9.7 9.5 9.5 9.8 10.5 10.8
100 60 30 14.3 13.4 2 13.8 14.75 FL 30 50 100 200 300 400

4.7 5.2 5.2 4.6 4.1 3.7 3.7 4.4 4.4 5.5 6.0
30 28 26 25 20 17 9.5 2 4.5 2 30

Spike S. Root 20" Maple 45' Lt. Sta. 12+72

B.M	14.01	1101.53		1087.52
13			19.1	1082.4
12			11.2	1090.3
11			1.6	1099.9
	14.57	1115.79	0.31	1101.22
10			5.9	1109.9
B.M.	16.50	1131.29	1.00	1114.79
9			11.9	1119.4
	16.33	1145.23	2.39	1128.90
8			15.5	1129.7
7			9.8	1135.4
6			5.5	1139.7
	15.58	1153.53	2.28	1142.95

Spruce 3 root 20" Maple 45' Lt Sta 12+72

15.3/23 19.2/20 18.2/18 18.1/12 18.9/6.5 18.3/4 19.1/2 20.0/9 22.9/30

14.5/37 18.6/31

8.0/38.5 12.6/31 13.2/26 14.4/25 13.2/22 12.6/16 13.7/7 11.2/5.5 14.2/2 9.9/30

+0.5/40 0.0/35.5 1.3/30 4.4/26 3.3/25 2.8/24 3.5/18 4.1/11 2.2/8 1.6/5 0.1/4 0.3/30

3.9/40.5 6.7/36 8.8/27 7.7/24 7.3/22 7.8/16.5 8.8/9 6.5/7.6 5.9/4.5 5.3/4 5.4/9 6.1/28 30

Iron pipe 25' Rt Sta 9+35

8.1/35 9.3/26 13.5/21 13.0/13.5 13.4/8 14.2/4 11.9/1 11.9/4 11.5/10 13.2/20 14.0/30

17.1/18 16.9/17 16.1/11 16.3/7 18.1/3.5 15.6/2.5 15.5/1 15.7/5 17.8/18 18.8/30

10.4/35 11.3/28.5 15.1/21

6.6/35 8.0/25 8.9/20 11.0/19.5 10.0/14 10.3/8 11.7/3 9.8/9 9.8/1 10.3/10 12.0/30

10.3/35 0.7/25 0.6/23 4.9/15.5 3.9/9.5 4.3/6 5.5/1.5 3.7/1.5 4.2/1.5 5.8/30

		1158.53		
5+50			13.8	1144.7
5			5.4	1153.1
B. M.	15.02	1165.14	8.41	1150.12
4+50			4.0	1161.1
B.M.	14.85	1174.45	5.54	1159.60
4			6.9	1167.6
3+15			1.0	1173.5
3	4.54	1178.61	0.41	1174.04
3			5.5	1173.1
2+50			8.8	1169.9
2			13.8	1164.8
1.50			18.4	1160.2
	0.52	1163.95	15.18.	1163.43
1			10.1	1153.9
0+50			15.7	1148.3

8.4 / 35 — 9.6 / 22 — 14.6 / 15 — 13.7 / 12 — 14.2 / 3.5 — 15.2 / 1.5 — 13.8 / 4 — 13.2 / 5 — 15.1 / 30

11 / 35 — 2.3 / 25 — 7.7 / 15 — 9.1 / 11 — 10.7 / 5.5 — 6.4 / 1 — 5.4 / 2 — 8.5 / 30

Spike N. side 20" Apple Pt sta 5+00 1' above ground

0.2 / 30.25 — 8.4 / 15.5 — 7.8 / 11.5 — 8.5 / 6 — 4.0 / 2 — 7.1 / 30

Iron pipe 25' Rt sta 4+45

2.7 / 35 — 4.0 / 22 — 11.0 / 15 — 10.6 / 10 — 10.9 / 5 — 6.9 / 2 — 6.9 / 4 — 9.4 / 30

6.3 / 35 — 1.1 / 25 — 3.3 / 9 — 6.0 / 7 — 5.5 / 4 — 6.0 / 4 — 5.4 / 6 — 8.0 / 30

6.4 / 30 — 8.3 / 6 — 13.8 / 4 — 13.4 / 6 — 14.6 / 11 — 11.1 / 15 — 12.8 / 30

11.2 / 30 — 13.2 / 6 — 18.4 / 2 — 18.8 / 1 — 18.6 / 5 — 19.6 / 13 — 16.5 / 18 — 17.3 / 30

Top of Stake 1+50

3.4 / 30 — 3.9 / 13.5 — 11.1 / 2.5 — 10.7 / 2 — 10.2 / 2.5 — 11.1 / 16 — 7.3 / 20-30

8.3 / 35 — 9.4 / 25 — 16.5 / 12 — 15.8 / 7 — 15.7 / 2 — 16.8 / 15 — 14.6 / 19 — 15.6 / 30

		1163.13		
0+00				
	0.55	1148.31	16.19	1147.76
0+00			6.2	1142.1
-25			9.5	1138.8
-50			13.5	1134.8
-100			17.0	1131.3
-150			19.7	1128.6
B.M			3.63	1144.68

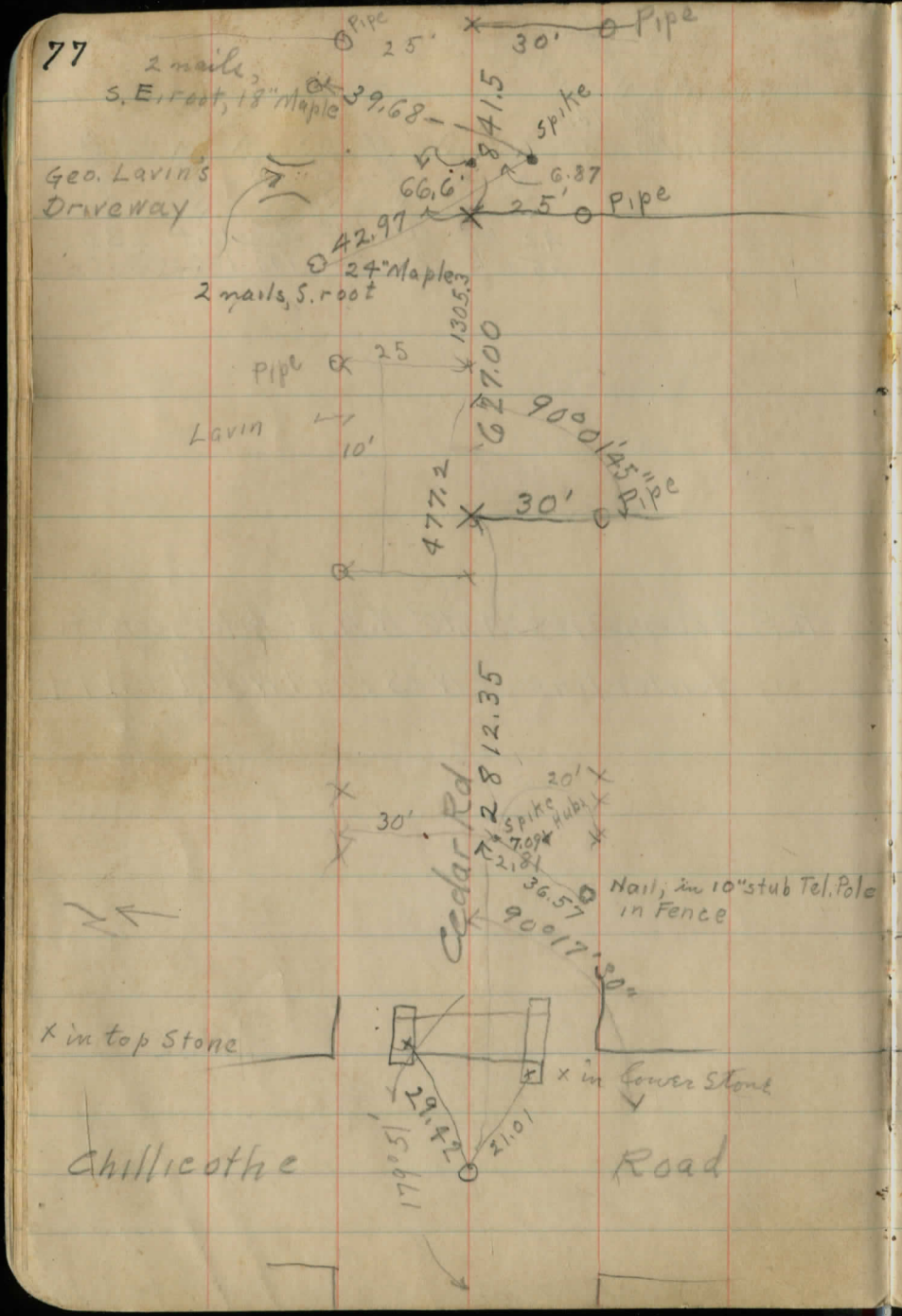
1157.3 / 6.7 / 150

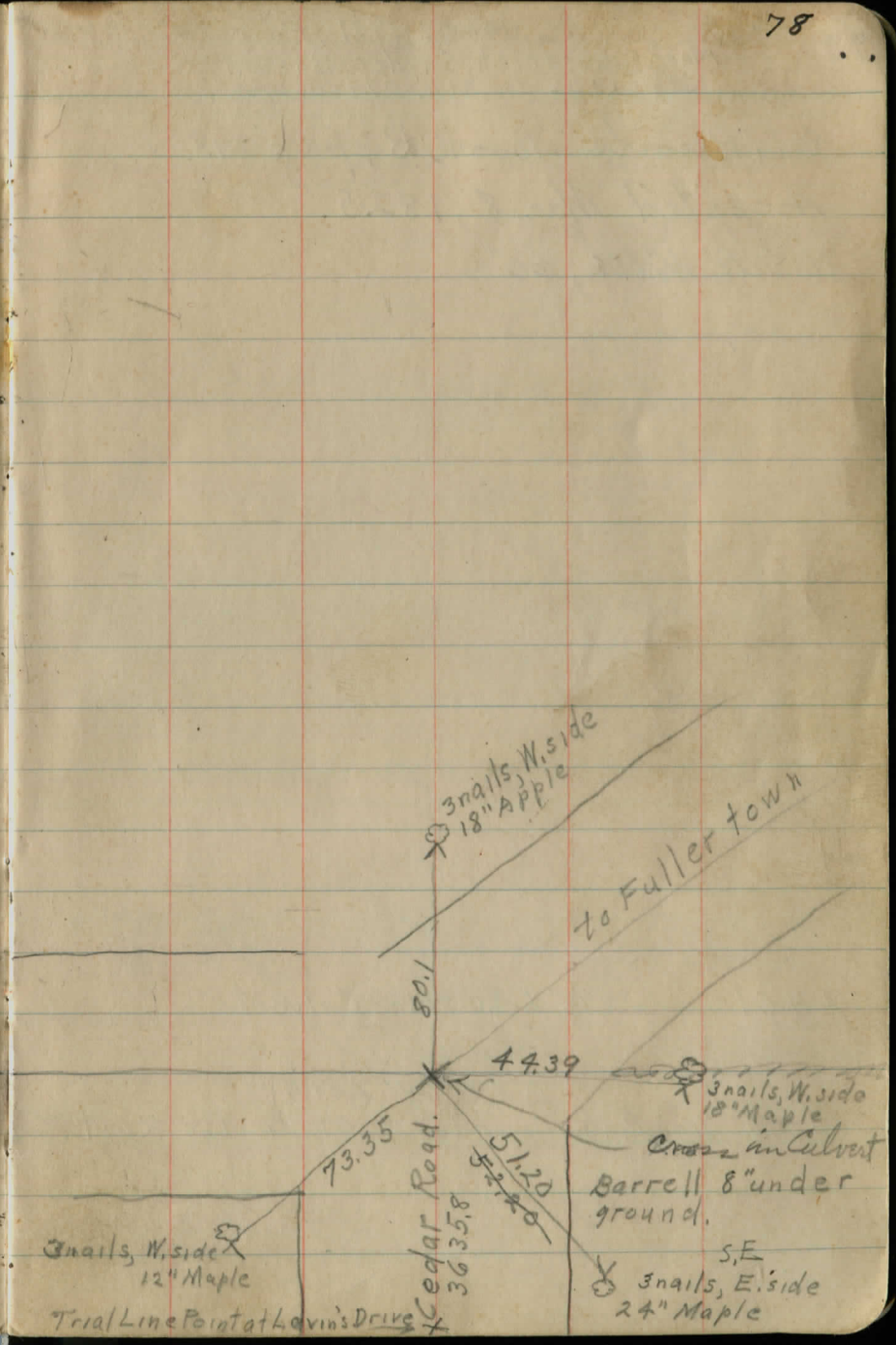
1152.5 / 11.5 / 100

1147.9 / 16.1 / 50

1144.1	1142.1	1140.2	1136.1	1132.7	1129.9	1125.3
4.2 / 25	6.2 / ℄	8.1 / 2.5	12.2 / 50	15.6 / 75	18.4 / 100	23.0 / 150

R.P. iron pipe 43.10' N.W. of intersection of centerline of N&S road with ℄ of E&W rd.


Pipe
25'
30'
Pipe
2 nails,
S. E. root, 18" Maple
39.68
41.5
spike
Geo. Lavin's
Driveway
66.6'
6.87
2.5'
Pipe
42.97
24" Maple
2 nails, S. root
1305.3
Pipe
25
Lavin
10'
627.00
90° 0' 45"
Pipe
30'
477.2
2812.35
Cedar Rd.
20'
30'
spike
Hub
7.09
2.81
36.5'
Nail, in 10" stub Tel. Pole
in Fence
90° 17' 30"
X in top Stone
X in Cover Stone
29.42
21.01
179° 51'
Chillicothe
Road


3 nails, W. side
18" Apple
to Fullerton
80.1
44.39
3 nails, W. side
18" Maple
Cross in Culvert
Barrell 8" under
ground.
73.35
51.20
S. E.
3 nails, E. side
24" Maple
3 nails, W. side
12" Maple
Cedar Road.
36.35.8
Trial Line Point at Lavin's Drive

June 3, 1931, Fair, 80°
Marks, Goodrich, Snyder, Barton.
Sta 62+36 to Sta. 87+00

Road Records Book B, page 218
Accepted Mar. 8, 1825
Statute Width, 60'

See Pg 91-92

FCP

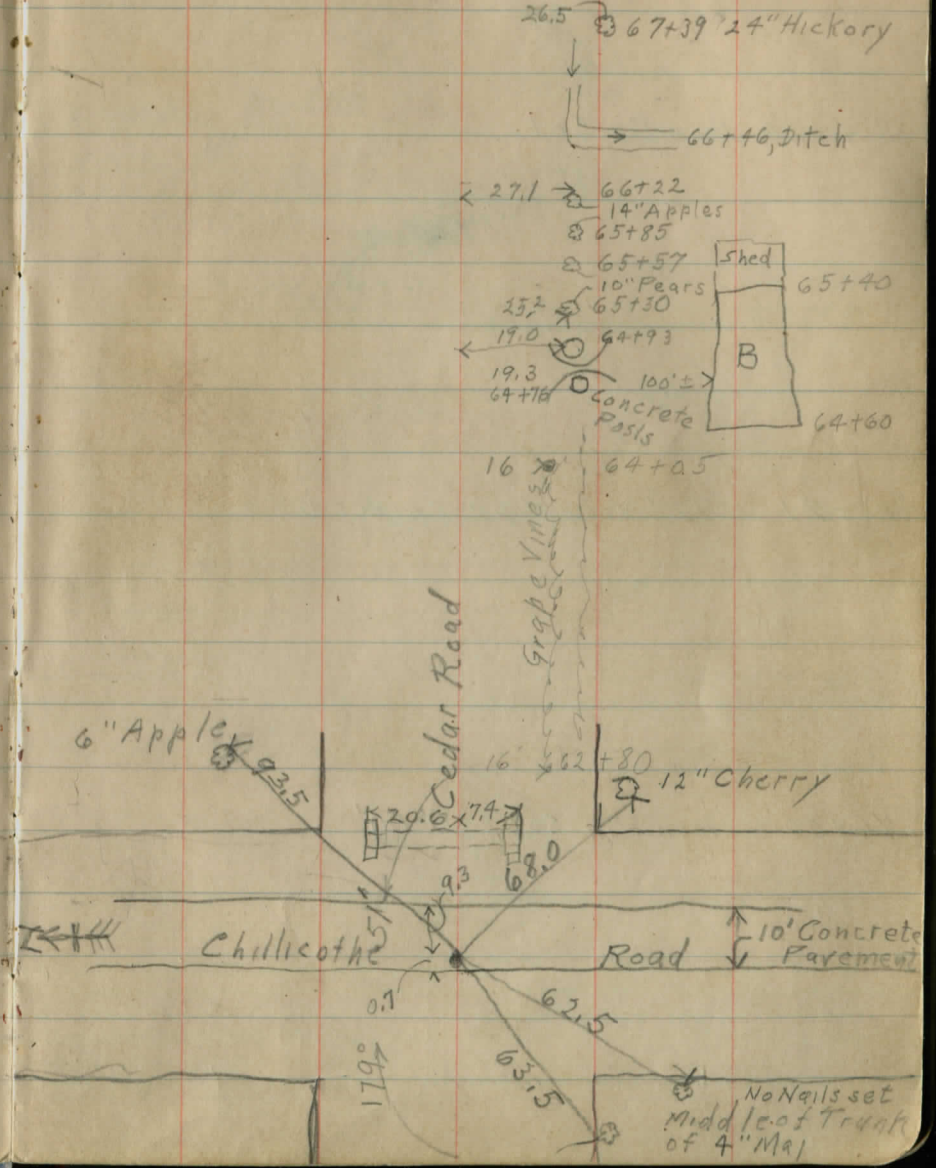
62+61 2½' X 3.0 Stone Culvert

Δ = 0°09' Left

62+36.0 Iron Pin in Concrete, ℄ Chillicothe Road.

73+68 20" Maple ⊙ 25.3

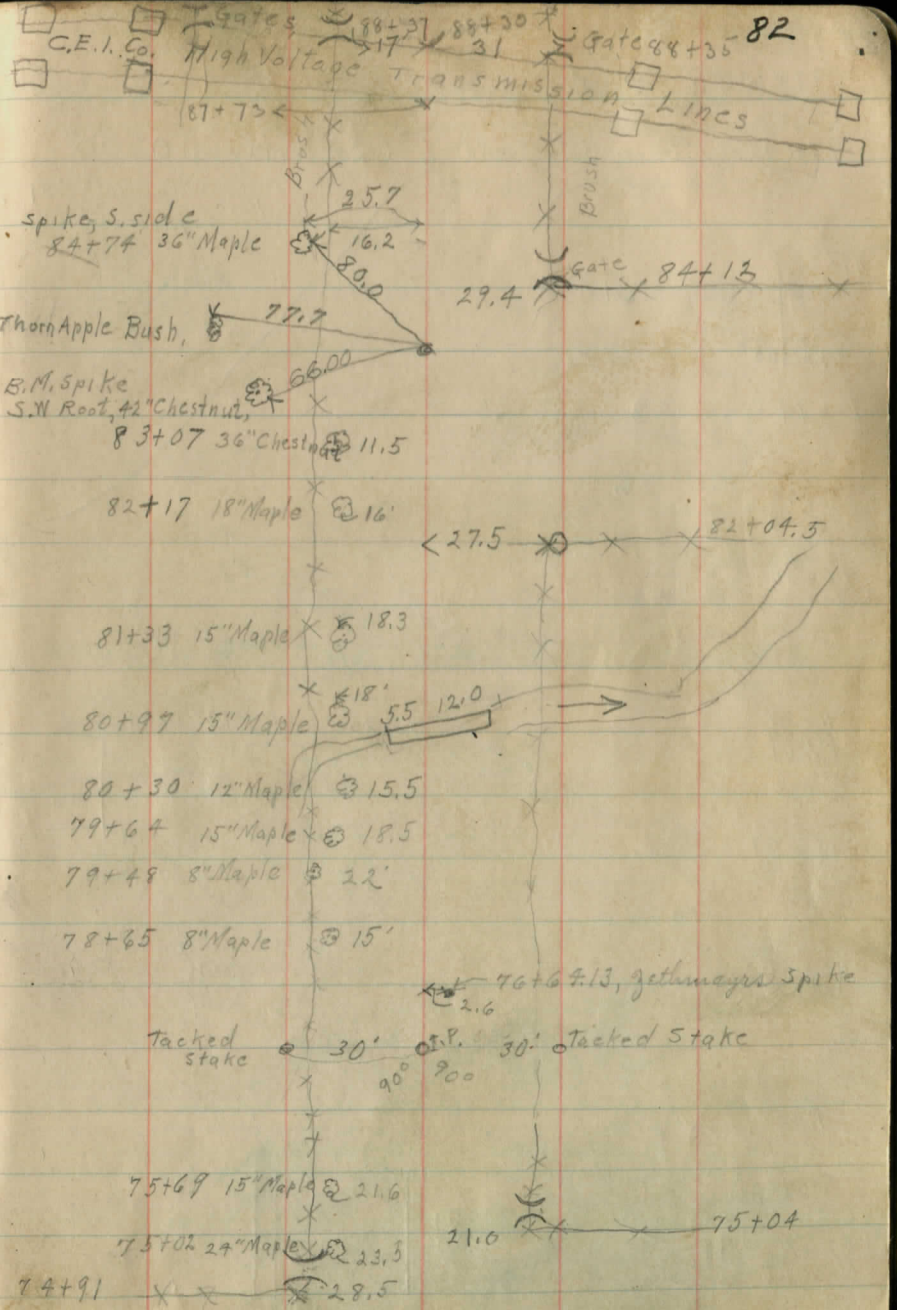
73+04 27" Maple ⊙ 24.5



8 4+00 Iron Pin Set.

80+71 12" V.t. Pipe Culvert

76+50 Iron Pin Set. 0°00'



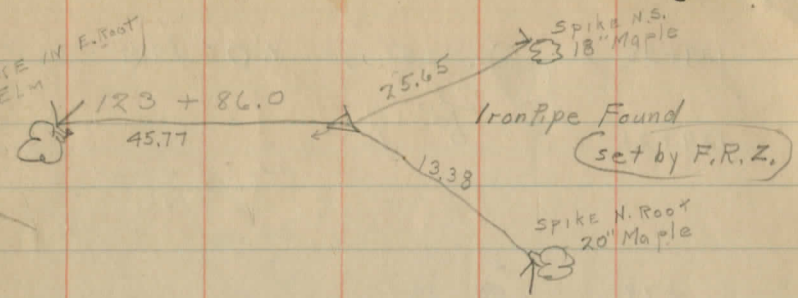
97+93 8" Cherry 25 >
97+63 30'
97+50 Drive
97+42.4 Iron Bolt Found (Zeth Mayrs) 0° 00"
Post tune 10-24 31
Snyder
Salem
Fair
97+28
97+16 31
97+00 2' Maple
65±
96+94 15" Maple 28
96+70 15" Maple 28
96+38 15" Maple 26'
96+30 Apple Stub
94+30 12" Vitrified Culvert
18'
91+94
91+64
91+61 No.
91+55
6" Maple
23 15" Apple
91+75 Drive
35 2' Maple
70±
No
91+37
91+16 35 30" Maple
90+50 34 2' Maple
P.L.
89+20
Bottom Slab - Concrete - Poor
Sandstone Walls - Fair
Concrete Slab - Good
℄ Culvert 88+88.0
Span 27
Height 3.0
24'
Poor Condition

103+02
102+89
102+72
102+61 Drive
102+48
9' 6" Apple
16'
3" Maple
31
4" Apple
28
4" Apple
102+39
House
16 3" Maple 102+31
102+19 T.P. 18
16 2" Maple 102+13
100'±
102+09
Spike S.E. Root
24" Maple
34.53
97+42.4 A=0°00'
37.55
Iron Bolt Found Set by F.R.Z.
Spike in S.E. Root 30" Maple
96+75.60
25.0
Iron Pipe
100+05.0 O.T.P. 18'
32
16
2" Maple
2' Apple
101+97
99+41 8" AP. 27
99+9 8" AP. 27
8" Apple
98+54 27
98+23 6" Cherry 25
98+21 6'
98+16 8" Ash
16 4" Elm 98+24
16 6" Hickory
98+13 T.P. 17

Fence × 28 10" Cucumber
111+31
111+07 ○ T.P. 19
109+58 ○ T.P. 18
108+80 Iron pin set Δ = 0° 00"
8" Maple ○ 23
108+57
1' Cucumber ○ 21
108+31
Pin ○ T.P. 15
108+15
1' Maple ○ 21
107+91
3" Ash ○ 18
107+43
8" W. Ch ○ 18
107+20
101+01
P.L. 106+89 Fence ○ 23 10" Mpl
106+24 W. Ash ○ 15 15
8" W. Apple
106+17
105+97 Wild Apple 8"
105+89 ○ 13
Brush
Top of Bank
22
Orange Hedge
Group of Elms
105+49
105+15 T.P. ○ 13
Twin Elm 8" each
Poor Cond. Sand Stone Culvert
104+67 104+64 Cul
11 21 18 10 17
1' Elm
104+39
103+89
Flag Stone Slab
This Culvert Carries No flood water And therefore will be O.K. for Rt 1 improvement
Fence 10" Apple ○ 21
103+78 ○ 14
103+53 8" W. Ch. ○ 14

123+00 12" Apl ○ 33
122+96
122+85
< 20' 4' Elm
122+60 < 80± 122+56
Iron Pipe ○ 30 × 30 ○ Iron Pipe
122+44 Drive
8" Mapl
121+45 ○ 32
120+58 < 13 20" Mapl
120+12 ○ T.P. 24
118+76 < 15 ○ 12" W. Ch
< 15 ○ 118+62 Fence
117+29 < 14 ○ 8" Mpl.
117+16 < 15 ○ Ash 8"
117+10
117+05 ○ T.P. 21 < 15 ○ 6" Maple
116+90 < 15 ○ 6" Ash
114+23 < 16 ○ 6 S. Maple
× 13 × ○ 1' V.T. Pipe Cul
114+12
T.P.
113+91 ○ 20
113+57 20 ○ 8" Elm
113+47 22 ○ 10" Apple

127+31 1" Mapl 29
127+26 16 8" Mapl
TP 18
127+22
127+12 29 16 3"
127+09 25
15 126+85
126+93 24
126+69 8" Mapl 24
126+60 8" Mapl 25
126+49 15
8" Mapl
126+24
126+23 15
126+6 8" Mapl 24 15
125+81 15" Mapl
125+64 8" Mapl 25
125+55 15 15" Mapl
6" Mapl
125+89 26
T.P. 23
125+26
8" Mapl
124+98 26
124+93 14 8" W. Ch.
8" Maple
124+82 25
124+80 13 2" Mpl
124+08 12
1" Maple
123+77 12
123+37 T.P. 27



123+0.0 Stake 15.0 Stake 5' Elm

Over

129+58 Fence 25 → 6'08" Elm

T.P. 0 16

129+21

+79 10" Mapl 28

+50 8" Mapl. 28

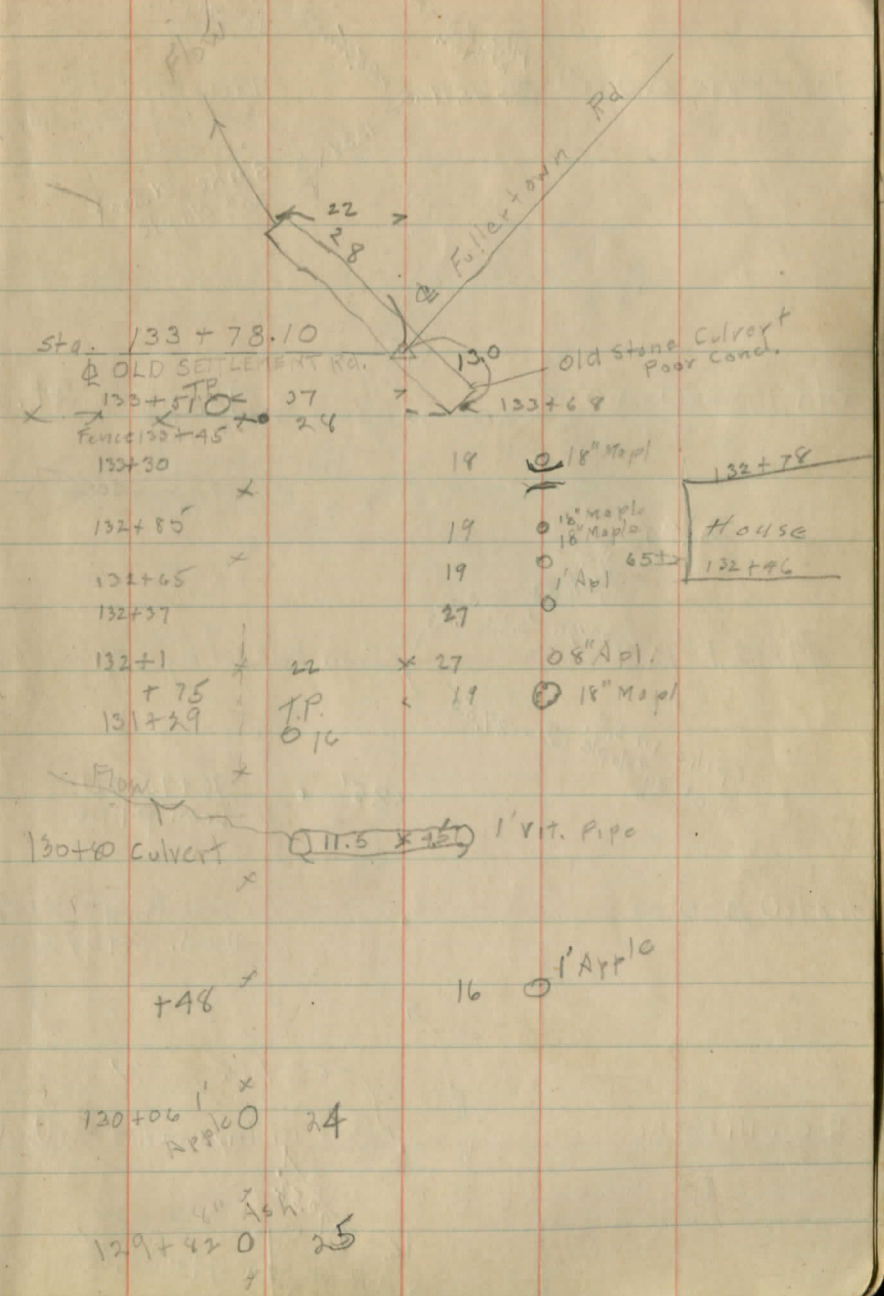
10" Ash 29

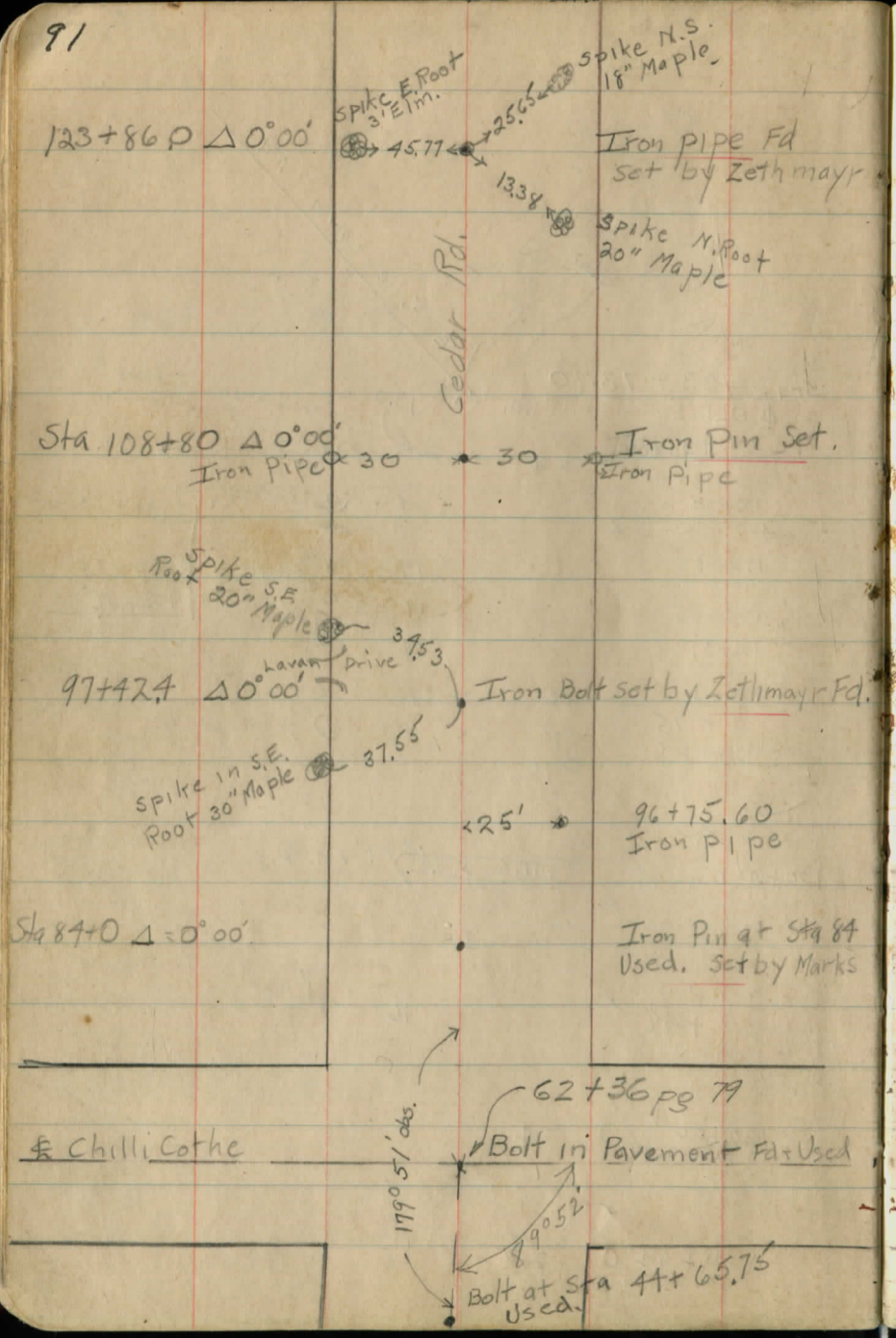
128+34

+89 8" Mpl 27

127+99 8" Mapl 29

127+52 2' Elm 29





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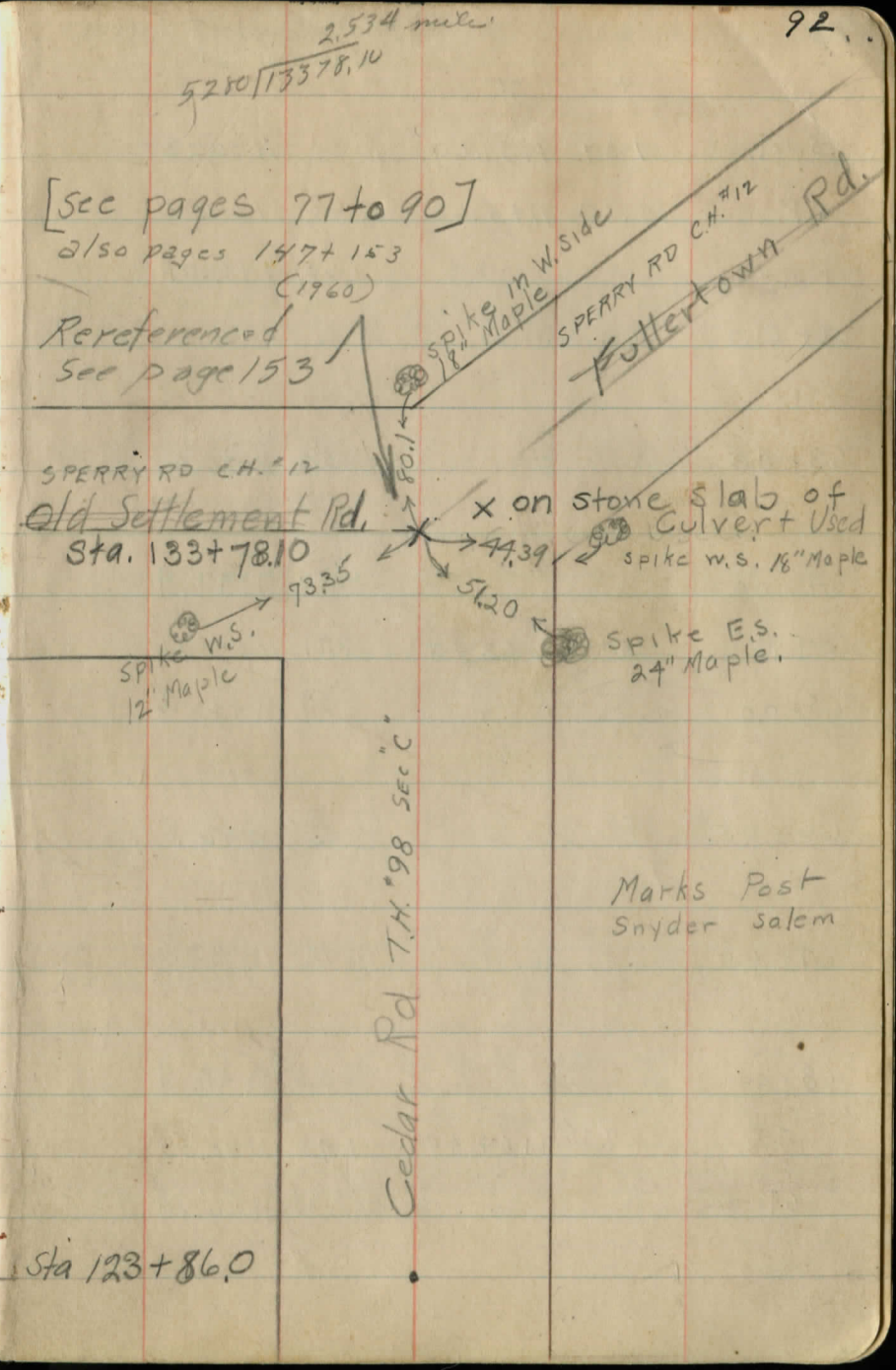
5280 | 13378.10



Post - Snyder - Salem
June 11 - 31
- clear - warm

	+	HI		
B.M.	1.37	1131.60		1130.23
T.P.	14.70	1145.62	0.68	1130.92
B.M. - 3			3.61	1142.01
62+61.0	Culvert		5.2	1140.4
63+0.0			5.0	1140.6
64+0.0			3.7	1141.9
T.P.	5.57	1148.48	2.71	1142.91
65+0.0			5.9	1142.6
66+0.0			5.65	1142.8
67+0.0			4.9	1143.6
68+0.0			3.6	1144.9
T.P.	7.85	1154.40	1.93	1146.55
69+00			7.85	1146.5

N. side

S. side

[500± S of Cedar Rd.]

Staple E. Root 29" Maple sta 20+70 Chillicothe Rd.

X S.W. Cor. N.W. Proj. of Culvert E.S. Chillicothe Rd. Across Cedar Rd.

1140.0 1138.8 1136.3 1135.4 1139.4 1142.0 1142.0 1140.9 1140.4 1140.4 1141.7 1139.1 1136.2 1133.7 1131.1 1125.1

5.2 6.8 9.3 9.2 6.2 3.6 3.6 4.2 5.2 5.2 3.3 3.9 6.5 10.3 11.9 14.0 16.8 30.6

100 50 25 20.6 20.6 20.6 19.0 19.0 ℄ 5.6 5.6 7.4 7.1 7.4 15.0 50.0 140.0 30.0

3.6 3.4 6.0 6.0 5.0 4.6 5.0 5.3 7.3 7.2 5.7 6.5

25 24 22 18 9.5 5.2 ℄ 7 10 12 15.5 30

4.4 1.6 4.8 4.8 5.4 4.5 3.3 3.7 4.3 5.7 3.9 4.4 4.9

10 24 19 16 16 11.5 3.0 ℄ 25 11.5 15.5 24 30

4.1 4.6 7.3 6.5 6.0 5.4 5.9 6.6 6.3 6.9

30 23 16 14 10 3 ℄ 8 15 30

5.7

7.3 5.0 6.6 5.9 5.3 5.65 6.2 7.7 6.8 7.8

30 26 16 12.5 5 ℄ 7 10 13 30

3.7 3.7 5.6 6.0 5.3 4.6 4.9 5.4 6.2 5.3 6.2

30 27.5 14 13 10.5 2 ℄ 7 10 13 30

2.0 2.6 4.6 5.3 4.6 3.6 4.1 4.8 4.3 4.4

30 24 13 0.5 8 ℄ 5 8 10.5 30

5.0 5.8 9.0 9.7 8.2 7.9 7.85 4.4 9.4 8.0 7.8

30 21 11 10 6.5 ℄ 6 9 13 30

	+	⊼	−	Elev
69+80.0		1154.40	6.4	1148.0
70+0.0			6.3	1148.1
71+0.0			4.9	1149.5
T.P.	10.46	1160.46	4.40	1150.00
71+50.0			10.0	1150.5
72+0.0			9.2	1151.3
73+0.0			6.8	1153.7
B.M.			1.55	1158.91
74+00			3.7	1156.8
T.P.	7.35	1167.68	0.13	1160.33
75+0.0			7.3	1160.4
76+00			5.3	1162.4
76+70			3.9	1163.8

N. side

S. side

5.8/30 7.9/13.5 8.5/12 8.5/10 7.0/5.5 6.4 ℄ 7.3/7 8.1/10 7.9/6 7.8/3.0

5.5/30 6.7/13 8.1/10 8.1/9 6.7/7.0 6.3/℄ 7.1/7.5 7.7/10 7.2/19 7.0/30

2.5/30 3.1/19 5.5/11 6.9/9 6.9/8 5.4/6 4.9/℄ 5.8/8 6.3/9.5 4.2/19 4.7/30

8.2/30 9.4/17 11.1/11 12.1/9 12.1/8 11.0/7 10.0/℄ 10.7/7 11.6/9.5 10.6/19 11.9/25 12.7/30

8.9/30 9.3/23 10.3/13 11.3/12 11.3/10 9.8/8.0 9.2/℄ 10.0/6 10.3/9 11.3/17 11.7/30

7.1/30 6.5/19 7.3/16 7.1/13.5 8.1/12 7.2/9 6.8/℄ 7.2/2.5 8.0/4 7.1/6 6.5/10 5.8/30

Spike in S. Root of 24" Maple N.S. Rd Sta. 73+70 [2.5 N. ℄

1.5/30 1.2/21 2.1/17 4.7/12.5 4.0/11 3.1/5 3.7/℄ 3.8/1.5 4.6/3.5 0.8/8.5 1.0/30

7.7/30 7.3/15 8.1/14 9.1/12 7.4/11 6.9/3.5 7.3/℄ 7.6/3.0 8.2/5 6.4/10 6.4/19 6.2/30

6.0/30 6.0/26 4.7/22 6.1/13 6.8/12 5.4/10 5.0/2 5.3/℄ 6.0/4 6.8/7 5.8/9 5.6/30

3.4/30 3.6/25 3.4/21 3.7/14 4.6/11 5.4/9 7.8/6 3.9/℄ 4.8/6 5.7/8 4.4/10 3.8/16 4.1/30

1167.68

77+00			5.0	1162.7
78+0.0			9.2	1158.5
79+0.0			11.7	1156.0
T.P.	5.10	1160.33	12.45	1155.23
80+0.0			5.8	1154.5
B.M.			4.91	1155.42
80+71		Culvert	6.5	1153.8
81+00			6.7	1153.6
82+00			6.2	1154.1
T.P.	2.35	1161.65	1.03	1159.30
83+00			2.5	1159.2
84+00			4.4	1157.3
85+00			8.6	1153.1

N. Sidg

3.4 / 30	3.9 / 20	4.5 / 14	5.5 / 12	5.5 / 11	6.4 / 9	5.6 / 6	5.0 / E	5.8 / 6.0	6.5 / 9.0	5.5 / 11	4.3 / 16	4.2 / 25
9.3 / 30	8.3 / 24	7.9 / 15	10.1 / 11	10.8 / 10	10.8 / 9	9.7 / 6	9.2 / E	10.1 / 7.	11.1 / 9	9.8 / 11	8.0 / 2.2	7.7 / 30
11.4 / 30	11.2 / 23	12.5 / 10	13.5 / 9.0	12.4 / 6	11.7 / E	12.5 / 8.5	13.6 / 11	12.6 / 12	12.4 / 20	12.4 / 30		
7.0 / 25	7.0 / 20	5.9 / 15	6.7 / 6	7.2 / 5	6.2 / 3	5.8 / E	5.6 / 2.5	6.3 / 6	7.7 / 11	6.4 / 13	5.4 / 25	

Spike S. Root 30" Maple 50' Left Sta 80+30

1152.6 1151.9 1151.9 1151.0 FL 1152.8 1153.0 1153.0 1153.7 1153.8 1154.2 1153.4 1151.9 FL 1151.2 1152.0 1147.6 1145.0 1141.3

7.7 / 138	8.4 / 50	8.9 / 25	9.3 / 7	8.0 / 7	7.3 / 7	7.3 / 6	6.6 / 2.5	6.5 / E	6.1 / 3	6.9 / 9.5	8.4 / 10.3	9.1 / 10.3	10.2 / 35	12.7 / 100	15.3 / 150	19.0 / 250
6.1 / 30	6.4 / 21	7.7 / 12	7.4 / 5	7.8 / 4	7.8 / 3	6.9 / 1	6.7 / E	6.3 / 5.0	7.2 / 13	8.0 / 17	8.5 / 25	8.5 / 30				
3.5 / 30	3.5 / 19.5	3.5 / 13	4.9 / 6	6.6 / 1	6.2 / E	4.9 / 8	5.4 / 13.5	6.0 / 16	5.5 / 19	4.9 / 25	4.9 / 30			
2.0 / 30	1.9 / 19	1.3 / 8	2.2 / 5	2.5 / E	3.6 / 2	2.8 / 4.5	2.3 / 10	3.0 / 14.5	3.7 / 17	2.5 / 19	2.4 / 30			
4.7 / 30	4.4 / 17	3.9 / 19.5	5.2 / 8.5	4.4 / E	5.4 / 1.0	4.7 / 4.5	4.3 / 9.5	4.8 / 14.5	5.5 / 17	4.6 / 19	4.3 / 30			
7.2 / 25	6.7 / 15	6.5 / 3	8.6 / E	9.5 / 1	8.7 / 5.5	8.2 / 6	8.7 / 13	9.6 / 15	6.9 / 19	8.5 / 30				

	+	⊼	−	Elev
		1161.65		
T.P	7.42	1158.04	11.03	1150.62
			12.6	1145.4
86+00			~~11.4~~	~~1146.6~~
T.P.	6.51	1152.80	11.75	1146.29
			16.5	1136.3
87+00			~~10.5~~	~~1142.3~~
T.P.	7.49	1145.23	15.06	1137.74
87+50			13.0	1132.2
T.P.	5.21	1136.32	14.12	1131.11
88+00			6.0	1130.3
		Ground.	8.4	1127.9
88+88.0		Culvert - Sandstone & Concrete		
89+00			9.5	1127.8
89+35			7.2	1129.1
T.P.	13.71	1144.54	5.49	1130.83
89+55			14.0	1130.5

Post snyder salem June 12 31 warm clear

N. Side

S. Side

Sta 86+00

6.9/40 5.7/30 6.8/16 6.8/9 12.6/℄ 11.4/3.5 11.0/8 11.4/13 12.3/14 7.6/22 7.5/30 7.5/40 6.7/40

27.2/40 13.2/30 10.9/20 11.9/8 16.6/1 16.5/℄ 16.4/2.5 15.0/7 15.7/12 16.3/14 15.4/14.5 11.3/19 6.7/24

18.4/50 16.4/40 13.8/20 12.2/12 11.3/3 13.0/℄ 12.0/1.5 11.6/9.5 12.6/15 13.1/16 11.8/17 6.0/29 4.9/40

10.5/40 10.4/35 8.6/16.5 6.0/℄ 5.7/2 6.1/3 5.5/6 5.0/11 5.9/17 6.6/25 7.7/35 7.5/45

VP stream ← 10.5/150 19.3/50 Flr. 12.8/℄ SIB 11.9/℄ COM H. WALL 7.4 7.6/0.9 8.8/0.9 7.1/8 6.7/13 7.4/19 8.6 7.2/23 7.2/24 SIB 10.2/24 FL. 13.6 11.2 2.7 14.9/50

15.9/100 19.0/200 24.1/300

12.3/40 11.1/16.5 9.5/℄ 7.3/6 6.6/13 7.3/19 10.5/25 13.0/40

6.9/40 9.0/25 7.7/℄ 7.6/2 6.5/7 6.1/11.4 7.4/19 9.4/30 10.9/40

17/40 32/25 14.0/℄ 15.7/1.2 14.1/3 13.4/11 14.6/17 13.6/19.5 11.5/24.5 8.9/32 8.9/40

		1144.54			
90+00			12.2	1132.3	
B.M.+T.P	8.45	1152.47	0.52	1144.02	Spike
91+0.0			9.3	1143.2	
91+40			6.7	1145.8	
92+00			9.2	1143.3	
T.P.	1.34	1142.50	11.31	1141.16	
93+00			3.5	1139.0	
94+00			6.3	1136.2	
94+30	V.t. Culvert		6.5	1136.0	

N. side S. side

0.0/40 17/21 12.2/℄ 11.5/3 11.1/9 12.3/15 5.3/25 4.8/30 5.5/40

In N. Root 30" Maple P.L. S. side at sta 90+50.0

3.3/40 4.8/12 9.9/1 9.3/℄ 8.7/6 10.1/12 6.0/17 5.6/40

4.3/40 5.0/14 4.6/6 7.1/2 7.1/1 6.7/℄ 6.0/5 7.2/12 5.5/14 3.9/35

7.0/40 6.8/9 10.3/3 10.3/2 9.2/1 9.2/℄ 8.7/6 9.3/11 10.1/12 7.6/15 5.9/40

3.6/35 2.2/7 4.6/3 3.5/℄ 2.7/5 3.4/10.5 4.3/12 4.3/13 2.7/16 1.5/21 1.7/35

6.7/35 7.1/4 6.3/℄ 5.1/4 4.6/9 5.1/13 6.4/16 6.9/35

1137.5 1135.4 1133.7 1134.8 1136.0 1136.0 1137.0 1137.4 1136.8 1135.4 1134.2 1133.5 1133.0

0.9/12.6 7.1/23 8.5/2 F.L. 1.7/2 6.5/2 6.3/℄ 5.5/16 5.1/6 5.7/12 7.1/16 P.L. 8.3/18 F.L. 9.0/18 9.5/2.5

1129.7 2.8/10.0 1126.9 16.0/20.0

	+	⊼	−	
95+00		1142.50	5.2	1137.3
T.P.	10.44	1149.76	3.18	1139.32
96+00			11.3	1138.5
B.M.			2.61	1147.15 Spike
97+00			8.0	1141.8
97+42			5.9	1143.9
97+75			7.2	1142.6
98+00			9.1	1140.7
T.P.	2.16	1140.59	11.33	1138.43
99+00			5.9	1134.7
100+00			10.6	1130.0

27/40 4.2/20 5.2/℄ 5.9/1 4.8/5 4.3/7 5.2/16 6.2/25 7.7/40

8.1/30 9.7/5 11.3/℄ 11.3/1 10.3/3 9.6/11 10.3/17 11.2/19 10.8/20 10.7/30

S,E
S.Root 24" Maple E. Side LAVIN Drive 30' N. ℄ Sta 97+63

2.6/30 4.5/19 6.0/7 8.3/1 8.0/℄ 7.0/9 7.8/14 8.3/16 7.6/17 7.6/30

3.0/30 5.0/24 5.9/9 5.9/℄ 5.9/6.5 6.6/12 7.3/14 6.5/16 6.9/30

3.4/30 4.4/16 6.6/4 7.2/℄ 7.0/7 7.6/12 8.4/14 7.2/16.5 7.5/30

5.1/30 5.5/11 9.8/2 9.1/℄ 8.8/6 9.2/11 10.1/13.5 8.0/17 8.2/30

1.2/30 2.0/16.5 1.4/14 7.0/6 7.0/4 6.1/3 5.9/℄ 5.6/4 6.3/9 7.5/10.5 4.5/16 3.1/30

7.6/30 8.2/18 10.5/8 10.6/6 11.9/5 11.1/4 10.6/℄ 10.3/3 11.0/8 12.0/11 9.4/16 8.6/30

	+	⊼	−	
T.P.		1140.59		
T.P.	0.65	1129.23	12.01	1128.58
✓ 101+00.0			3.6	1125.6
✓ 102+00			7.3	1121.9
T.P.	2.70	1123.05	8.88	1120.35
✓ 103+00			6.2	1116.9
✓ 104+00			8.1	1115.0
T.P.	4.52	1118.38	9.19	1113.86
✓ 104+64	℄ Culvert		4.7	1113.7
105+00			.52	1113.2
✓ 106+00			4.0	1114.4
T.P.	11.27	1129.00	0.65	1117.73
✓ 107+00			10.9	1118.1

N Side ℄ S Side

34/30 33/11.5 49/9 49/8 41/6.5 3.6/℄ 41/7 59/9 37/10 24/15 1.9/30

79/30 77/11 89/9 89/8 79/6 7.3/℄ 80/6 83/7 7.5/8 54/14 38/30

48/30 37/13.5 79/8 70/7 64/6.5 62/℄ 70/7 27/14 2.5/30

86/30 80/20 44/8 81/℄ 86/6 92/8.5 8.2/9 9.3/13.5 9.8/30

1112.5 1110.6 1110.6 1109.6 1111.5 1112.9 1112.9 1112.5 1113.7 1113.0 1111.0 1109.7 1109.2 1107.9 1107.2 1105.8

59/200 7.8/100 7.4/35 8.9/11 Pl. 6.9/11 Slab 5.5/11 5.6/45 5.9/9.5 47/℄ 54/10 Slab 7.9/10 8.7/10 Pl. 9.2/25 10.5/75 11.2/100 12.6/200

7.8/30 7.7/23 4.2/5 5.8/2 5.2/℄ 4.8/4 5.1/11 7.8/26 8.7/30

4.0/30 3.8/23 4.6/15 4.6/6 4.4/5 4.6/3 4.2/2 4.0/℄ 3.6/4.5 4.6/1 4.2/13 5.7/25

5.4/30 5.4/21 11.7/9 10.9/1 10.9/℄ 11.8/6 7.8/12 7.9/21 7.4/25 7.7/30

	+	⊼	−	Elev
		112900		
T.P.	9.30	1137.26	1.04	1127.96
			5.16	1132.10
B.M.	70' Left	Sta	107+70	Spike S.E. Root 18" Beech
✓108+00			10.2	1127.1
✓108+80			4.3	1133.0
✓109+00			4.8	1132.5
✓110+0.0			9.8	1127.5
T.P.	2.06	1129.57	9.75	1127.51
✓111+00			8.7	1120.9
✓112+00			14.1	1115.5
✓113+00			15.7	1113.9
T.P.	3.14	1116.68	16.03	1113.54

N. Side

S. Side

52/30 56/27 49/14 84/15 105/10.5 99/4 102/E 107/3.5 67/10.5 65/17 71/20 64/2.5 70/30

40/30 35/25 45/14.5 43/12 53/11 40/4 73/E 53/5 45/8 47/25 52/30

38/30 45/14 56/11 44/4 48/E 53/4.5 49/7 50/19 53/30

64/30 64/23 68/16.5 99/14 94/13 84/7 98/E 100/1 100/2 71/6 67/21 68/30

38/30 40/28 37/22.5 85/14 80/6.5 83/1 87/E 85/2 40/6 30/12.5 30/18 35/30

125/30 125/26 127/14.5 148/15 137/12.5 135/7 141/E 144/1 144/2 121/8 112/13 113/20 113/30

Est. 169/30 167/26 161/14 165/13 158/11.0 157/E 162/1.9 161/5 165/16 167/50

		1116.68		
114+00			4.8	1111.9
	Post snyder + Salem		June 13-31 Clear + Hot	
114+12	Vit. Pipe Culvert		4.9	1111.8
T.P.	6.84	1118.07	5.45	1111.23
115+00			5.4	1112.7
116+00			4.7	1113.4
B.M.			5.23	1112.84
117+00			8.5	1114.6
T.P.	8.28	1124.50	1.85	1116.22
118+00			6.8	1117.7
119+00			3.7	1120.8
T.P.	11.10	1134.23	1.37	1123.13
120+00			11.9	1122.3

Spike

Left N. Side

Right S. Side

62/30 62/27 57/14.5 47/11.5 43/4 48/E 53/3 52/5 57/9 64/15 75/30

1109.8 1109.8 FL 1110.0 1111.23 1111.4 1111.8 1112.4 TP 1110.8 FL 1109.7 1108.7 1106.7 1105.7

69/200 69/25 67/13 54.5/13 53/12.5 49/E 43/3 59/9 70/9 80/25 100/125 110/200

Culvert

69/30 58/11 63/10 62/9 56/7.5 51/3.0 54/E 60/5 65/9 73/17 85/30

41/30 50/12 54/11 59/10 50/9 42/3 47/E 46/3 49/9 46/5 51/22 64/27

N. Root 20" Hickory S.S.-50' Left Sta 116+10

50/30 37/27 33/19 33/16 40/15 40/14 33/12 29/6 36/E 24/3 23/16 48/40

54/30 41/28 75/30 69/19 89/17 79/16 72/10 76/A 42/3 82/1 68/E 87/25 87/30

91/30 107/28 44/21 56/19 56/18 49/17 44/10.5 53/3.5 28/2 37/E 43/16 51/26 52/30

105/30 119/20 132/18 133/17 119/8 122/3 116/2 119/E 125/2 123/15 119/30

	+	℄	−	Elev
		1134.23		
121+00			9.3	1124.9
122+00			3.7	1130.5
T.P.	10.01	1143.31	0.93	1133.30
B.M.			6.04	1137.27 Spike
123+00			7.8	1135.5
124+00			4.1	1139.2
T.P.	4.32	1135.89	11.74	1131.57
125+00			6.3	1129.6
126+00			11.5	1124.4
T.P.	1.01	1124.55	12.35	1123.54
127+00			4.1	1120.5
128+00			8.6	1116.0

85/30 88/20

102/19 102/18 93/16.5 85/10 91/5 96/4 96/2 91/1 93/E 83/12 85/25

88/27 68/21 68/19 59/18 53/11 60/6 65/4 37/E 30/4 27/12 27/25 32/30

N. Root. 50" Elm 21' Rt Sta 123+00 [In Front Yard]

67/30 69/24

96/20 85/18 80/12 85/8 94/5 78/2 78/E 73/12 64/13 64/20 74/40 Yard

31/30 39/14 62/13 62/14 49/12 45/7 62/3.6 54/2 59/1 41/E 44/10 38/13 44/30

03/30 11/18 64/12 54/7 59/1 63/E 68/2 21/1 08/19 10/30

109/30 101/18 124/15 124/13 117/12 105/8 115/E 130/3 130/4 100/6 99/19 85/18 79/21 76/30

41/30 33/15 52/12 52/10 46/9.5 36/5 41/E 45/3 53/5 29/9 21/11 13/20 16/25 11/30

73/30 70/27 62/18 92/11.5 85/10 81/5 88/E 93/3 56/8 60/10 44/30

	+	⊼	−	Elev.	
		1124.55			
✓ T.P	5.33	1117.43	12.45	1112.10	
129+00			5.7	1111.7	
✓ 130+00			7.9	1109.5	
T.P.	3.34	1111.47	9.30	1108.13	
✓ 130+80	Vit. Pipe Culvert		3.6	1107.9	
✓ 131+00			3.8	1107.7	
✓ 132+00			3.9	1107.6	
T.P.	3.10	1110.18	4.39	1107.08	
133+00			4.6	1105.6	
B.M.			3.90	1106.28	Ref Spike
133+50			5.4	1104.8	
133+78.10		Culvert	4.7	1105.5	

N.S. Left ℄ S.S. Right

℄

25/30 25/26 3.3/17.5 6.3/12.5 5.8/11 5.3/5 5.7/℄ 6.1/1.5 6.9/2.43 6.9/4 5.4/7 4.6/10 2.8/21 1.8/30 1.3

8.6/30 8.5/25 7.9/22 8.3/14 8.7/12 8.2/10 7.6/5 7.9/℄ 8.4/1.5 9.2/2 9.3/4 8.1/6 8.1/7 7.4/10 2.0/24 6.2/30

1095.5 1094.4 1108.1 1113.7 F.L. 1103.5 T.Pipe 1104.6 1106.3 1108.0 1107.9 1107.5 1106.1 1105.2 1104.1 1105.5 1105.6 1104.6

1.6/200 12.1/150 9.4/75 7.8/30 8.0/11.5 6.9/11.5 5.2/11 8.5/8.5 3.6/℄ 4.0/2 5.4/4.5 6.3 Top Pipe/4.5 3.9/4.5 F.L. 6.0/25 5.7/100 3.9/200

5.8/30 5.4/22 4.7/14 5.3/13 5.3/11 4.2/10 3.4/5 3.8/℄ 3.9/3 4.6/4.5 5.7/30

4.7/30 4.7/22 4.6/14 5.4/13 5.9/10 4.3/8 3.6/2.5 3.9/℄ 4.3/9 5.6/6.5 4.6/9 4.5/16 4.1/20 3.9/3.9

2.5/30 2.5/22 3.2/14 5.7/13 3.9/6 4.6/℄ 5.2/5 4.0/7 3.9/15 3.6/30

S.W. 24" Maple 51.20' E. side From Mon. & Cedar Fullertown Rd.

4.1/25 2.5/30 6.1/25 4.8/10 5.4/℄ 6.1/3 5.4/7 6.4/20 6.4/30

1094.5 1100.0 1101.6 1103.2 F.L. 1104.1 Top Pipe 1105.1 1105.5 1105.0 1103.8 F.L. 1103.4 1103.7 1103.7 1104.9 1104.0

15.7/150 10.2/100 8.6 7.0/53 6.1/26 5.1/27 4.7/℄ 5.2/10 6.4/10 Top Pipe 6.3/10 F.L. 6.5/30 6.5/30 5.3/100 4.2/150

Fullertown Rd

℄

				Sta.	
0+50		1110.18	3.1	1107.1	133+78.10	on Cedar Rd.
0+75			2.1	1108.1		
1+00			0.6	1109.6		
1+10			0+00	1110.18		

N+South Road

0+50			5.0	1105.2	Sta 0+00 = Sta 133+78.10	Cedar Rd
1+00			5.2	1105.0		
1+50			5.2	1105.0		
2+00			7.0	1103.2		
2+50			9.5	1100.7		
T.P.	6.53	1113.33	3.38	1106.80		
B.M.			2.14	1111.19	spike	E. Root · 8" Maple S.E. Cor Fullertown Rd. & Drive to House South.

Slope Stakes,

	0.13	1111.32		1111.19	
			5.02	1106.30	
			5.11	1106.28	Rec'd
133				1105.6	5.12
132				1107.6	
	9.74	1117.59	3.47	1107.85	
131				1109.0	
130				1110.4	
129				1112.0	
	11.47	1128.84	0.22	1117.37	
128				1116.5	
127				1121.0	
126				1126.5	
	14.60	1143.34	0.10	1128.74	
125				1131.5	
124					1237.0
123					1234.9
			6.12	1137.22	
B.M.	0.11	1137.38		1137.27	Record
122					1129.9
121					1124.9
120					1122.8
			15.18	1122.20	

Sept. 10, 1931, Marks, Parks, Snyder. Fair, 90°

Between Fullertown Road and Drive to House South.

B.M. E. Root, 8" Maple, 75' Right, 134+00

R.R. spike, S.E. side 24" Maple, 18' R. Sta. 133+30

5.72	C 2.0 / 20.0	3.69	5.11	C 0.6 / 20.0
3.72	F 0.2 / 19.0	3.93	3.81	F 0.1 / 17.0
8.59	F 2.5 / 19.0	11.07 / 1106.52		F 2.6 / 16.0
7.19	F 1.3 / 26.5	8.47	7.07	C 0.1 / 17.0
5.59	C 2.8 / 27.5	2.78	1.83	C 3.8 / 21.0
12.34	C 1.1 / 27.0		8.86	C 3.5 / 19.0
7.84	F 0.3 / 26.5	8.16	6.13	C 1.7 / 16.0
3.34	F 1.3 / 28.0	3.63	2.11	C 0.2 / 14.5
11.84	C 4.7 / 31.0	7.14	7.68	C 4.2 / 14.0
6.34	C 3.4 / 31.0	2.90	3.70	C 2.6 / 14.0
8.44	C 2.0 / 29.5	6.42	6.74	C 1.7 / 13.0

Spike, W. Root, Elm, 20' R., Sta 122+95

7.48	C 1.0 / 24.5	6.50	5.54	C 1.9 / 15.5
12.48	C 1.1 / 25.5	11.42	11.22	C 1.3 / 15.5
14.58	C 0.3 / 21.0	14.32	15.18	F 0.6 / 13.0

Slope Hub. 120+00, Right.

94+30 15" Pipe Culvert.

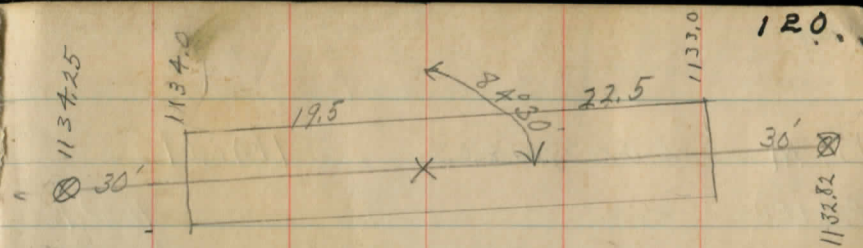
	1.88 1149.03	1147.15	
	11.28	1134.25	
	13.21	1132.82	

80+71 15" Pipe Culvert

B.M. 80+30 Left.	2.77 1158.19	1155.42	
	2.83	1151.36	
	7.00	1149.69	

130+80 15" Pipe Culvert

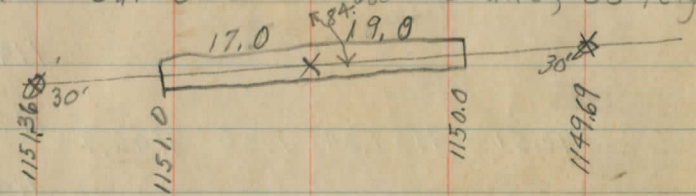
Slope Hub Left, 131+00	6.48 1113.00	1106.52	
	5.25	1104.75	
	7.65	1103.35	



S. E Root, 24" Maple, 30' L, 97+63

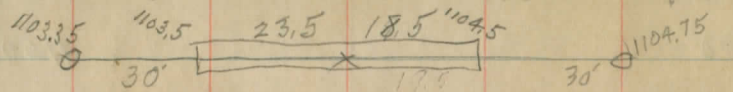
14.78 Cut 3'6" Stake, 30' Left.

16.21 Cut 3' 0" Stake, 30' Right



6.83 Cut 4' 0" Stake 30' Left.

8.50 Cut 1' 6" Stake 30' Right



8.25 Cut 3' 0" Stake 30' Right

9.65 Cut 2' 0" Stake 30' Left

Slope Stakes

B. M	6.02	1148.03		1142.01	
63+00					1139.1
64					1140.5
65					1141.9
66					1143.1
67					1144.2
68					1145.3
	10.51	1157.24	1.30	1146.73	
69					1146.5
70					1148.3
71					1150.0
71+50					1150.9
72					1151.9
73					1153.7
	9.06	1165.78	0.52	1156.72	
B.M	6.82	1165.73	6.82	1158.96	
				1158.91	record
74					1156.8
75					1160.0
76					1162.4
76+70					1162.0
77					1161.3

Sept, 15, 1931
D. Parks; T. Snyder
Cloudy warm Wind 80°

SHOVEL + Outfit moved on Job at 10 A.M across Cedar Rd.

X S.W. Cor, N. Parapet Culvert E.S. Chillicothe Rd.

8.93	8.40	C 0.5 / 20.0	8.59	C 0.3 / 20.0
7.53	6.06	C 1.5 / 19.5	6.75	C 0.8 / 20.0
6.13	5.31	C 0.8 / 18.5	6.21	F 0.1 / 20.0
4.93	5.77	F 0.8 / 18.0	6.45	F 1.5 / 17.0
3.83	4.60	F 0.8 / 16.5	4.96	F 1.1 / 16.0
2.73	3.63	F 0.3 / 16.0	3.74	F 1.0 / 16.5
10.74	8.79	C 2.0 / 19.0	10.51	C 0.2 / 19.0
8.94	8.73	C 0.2 / 18.0	9.63	F 0.7 / 16.5
7.34	5.78	C 1.5 / 20.5	7.09	C 0.2 / 18.5
6.34	5.57	C 0.8 / 18.0	7.79	F 1.5 / 17.0
5.34	6.57	F 1.2 / 17.0	7.98	F 2.6 / 19.5
3.54	3.28	C 0.3 / 18.5	2.56	C 1.0 / 20.0

Spike in S. root 24" Maple 25' N. of ℄ sta. 73+70

8.83	4.34	C 2.6 / 23.0	5.98	C 3.0 / 23.0
5.73	5.29	C 0.4 / 20.0	4.11	C 1.6 / 21.5
3.33	2.80	C 0.5 / 19.0	3.15	C 0.2 / 18.5
3.73	1.16	C 2.4 / 22.5	1.28	C 2.5 / 22.5
4.43	1.84	C 2.6 / 22.5	1.85	C 2.6 / 22.5

		1165.73			
T.P.	0.48	1160.20	6.01	1159.72	
78					1159.0
79					1156.8
80					1154.5
			4.83	1155.37	
B.M.	4.83	1160.25		1155.42	record
81					1154.0
	8.37	1164.02	4.60	1155.65	
82					1156.0
83					1158.0
84					1157.3
85					1154.3
	1.37	1153.33	12.06	1151.96	
86					1149.0
87					1142.3
			6.33	1147.00	
T.P.			6.33	1147.00	
B.M.			9.31	1144.02	record 1144.02

Slope Hub Rt sta. 78+00

		C 0.9			C 0.7
1.20	0.33	20.0		0.48	19.5
		FO.8			F1.4
3.40	4.20	17.0		4.83	16.5
		FO.4	3.84		C0.5
5.70	6.09	19.0		5.23	18.0

Spike in S. root 30" Maple 40' Lt. Sta. 80+30

		F0.1			F1.6
6.25	6.30	17.5		7.81	17.0
		C1.4			F1.4
8.02	6.66	20.0		9.39	17.0
		C1.9			C1.5
6.02	4.12	22.0		4.49	22.0
		0.0			F0.4
6.72	6.69	12.5		7.10	18.0
		C0.5			C0.9
9.72	9.18	20.0		8.87	22.0
		C3.3			C4.6
4.38	1.04	24.5		2.78	25.0
		FO.4			C4.4
11.03	11.43	27.5		6.65	32.5

Large rock 30' Rt. Sta. 87+00

Spike in N. Root 30" Maple 34' Rt. Sta. 90+50

T. P	5.15	1152.15		1147.00	
86					1148.00
87					1140.00
	0.44	1140.19	12.40	1139.75	
88					1132.0
	6.77	1135.97	10.99	1129.20	
89					1129.0
89+35					1130.1
89+55					1130.9
	11.25	1147.02	0.20	1135.77	
90					1134.0
			2.99	1144.03	
B. M.	6.63	1150.65		1144.02	record
91					1141.0
91+40					1143.0
92					1143.0
93					1140.5
	5.87	1144.07	12.45	1138.20	
94					1138.0
95					1139.5
96					1140.9
	7.95	1149.82	2.20	1141.87	
97					1142.4
97+42					1143.0
			2.66	1147.16	
B. M.				1147.15	record

Sept. 16 1931
D. Parks, H. Barton, T. Snyder, S. Merritt — Setting Slope stakes Sta. 37+ to Sta. 14+00

Large rock 30' Rt. Sta. 87+00

4.15	0.0	C4.2 / 24.5		1.58	C2.6 / 25.0
12.15	19.24	C2.9 / 18.0		5.46	C6.7 / 32.5
8.18	12.53	F4.3 / 18.0		11.10	F2.9
6.97	9.71	F2.7 / 5.0		10.63	F3.7 / 30.5
5.87	6.81	F0.9 / 4.5		10.14	F4.3 / 33.0
5.07	0.38	C4.7 / 10.0		1.76	C3.3 / 32.5
13.02	3.64	C9.4 / 24.0		7.08	C5.9 / 33.0

Spike in N. root 30" Maple 34' Rt. Sta. 90+50

9.65	1.76	C7.9 / 27.5		3.65	C6.0 / 30.5
7.65	2.59	C5.1 / 25.0		2.35	C5.3 / 26.0
7.65	5.17	C2.5 / 22.5		4.73	C2.2 / 23.0
10.15	10.32	F0.2 / 18.5		10.00	C0.2 / 17.5
6.87	8.69	F2.6 / 18.5		7.41	F1.3 / 18.0
4.57	5.84	F1.3 / 16.5		7.26	F2.7 / 18.0
3.17	2.75	C0.4 / 19.0		5.09	F1.9 / 17.0
7.42	3.72	C3.7 / 23.5		7.43	0.0 / 18.0
6.82	4.97	C1.9 / 27.0		6.87	F0.1 / 19.5

Spike in S. root 24" Maple 30' Lt. Sta. 97+63

Sept. 17, 1931
Cloudy, Warm. Wind 75°
W.C. Marks, D. Parks, T. Snyder

B.M.	0.35	1147.50		1147.15		Spike in S. Root 24" Maple 30' Lt, Sta 97+63				
97+75					1142.0	5.50	1.14	C4,3 25.5	5.33	C0,2 19.5
98					1140.7	6.80	2.26	C4,5 25.0	5.77	C1.0 21.0
99	1.07	1138.40	10.17	1137.33	1136.1	11.40	8.00	C3,4 23.0	10.17	C1.2 16.5
100					1131.3	7.10	5.63	C1,5 21.0	6.74	C0.4 16.0
101	0.20	1126.41	12,19	1126.21	1126.6	11.80	12,19	F0,4 18.5	11.36	C0.4 20,5
102					1121.9	4.51	4.02	C0.5 19.0	1.43	C3,1 23,0
103	4.59	1118.69	12.31	1114.10	1118.5	7.91	7.50	C0,4 20.0	5.84	C2,1 22.0
104					1115.0	Side stake Rt. Sta. 104+00 3.69	3,99	F0.3 19.0	4.94	F1.3 17.0
105					1114.6	4,09	7.77	F3,7 21.0	7.41	F3.3 18.0
106	15,40	1132,95	1.14	1117.55	1114.4	4.29	3,97	C0,3 19.0	4,67	F0.4 18,5
107			0.89	1132.06	1120.8	12,15	9,15	C3.0 24.0	11,71	C0,4 20.0
B.M.	5,41	1137,51		1132,10	record	Spike in S.E. root 18" Beech 70' Lt. Sta. 107+70				
108					1127,1	10.41	5,70	C4,7 26.5	6.47	C3,2 23,0
108+80					1131.0	6.51	3,47	C3.0 22,5	4.66	C1,9 21.5
109					1131.0	6.51	4,41	C2,1 21.5	5,31	C1,2 20.5
110					1127.5	10.01	6.36	C3,7 24.0	6.35	C3,7 24.0
111	0.28	1125,58	12.21	1125,30	1123.0	14,51	11.50	C3.0 23.5	10.97	C3.5 23,5
112					1117.4	8,18	8,30	F0,1 19.5	6,52	C1,7 19.5

		1125.58								
								F0.3		F0.4
113	7.12	1120.68	12.02	1113.56	1113.9	11.68	12.02	18.5	12.12	18.5
								F2.2		F3.1
114					1113.3	7.38	9.55	18.5	10.44	20.0
								F0.9		F1.6
115					1112.7	7.98	8.90	18.5	9.62	17.0
								C0.1		F0.3
116			7.80	1118.88	1113.4	7.28	7.14	19.0	7.58	19.0
B.M	7.80	1120.64		1112.84	record	Spike N. Root 20" Hickory 50' Rt. Sta. 116+10				
								C1.8		C0.7
117					1114.6	6.04	4.26	21.0	5.38	19.5
								F0.3		F0.8
118	9.11	1126.50	3.25	1117.39	1117.7	2.94	3.25	20.0	3.71	15.5
								F1.0		F0.2
119					1120.8	5.70	6.65	20.0	5.93	14.5
			4.32	1122.18						
				1122.20	W.C. Marks	T.P.				

Slope Hub Rt. Sta. 120+00

Culvert, 62+61 Stakes Set 40' Each

sept. 18, 1931. Fair, 75° Marks, Parks, Snyder Rf.
side of ℄ of Cedar Road, 25' E. of ℄ of Chillicothe

Graded for Flow Line 3.0' below ℄ of Chillicothe Rd.

B.M.	9.82	1131.12		1121.30	
48					1123.00
47+75					1123.15
B.M.	0.67	1142.68		1142.01	
T.P.			4.20	1138.48	
61					1134.75
60					1131.50
59					1128.50
	8.81	1136.34	15.15	1127.53	
58					1127.16
57					1127.75
56					1130.00
55					1130.50
			4.93	1131.41	
B.M	4.93	1136.36		1131.43	record
54					1127.10
53					1121.70
	0.84	1121.59	15.67	1120.75	
52					1116.30
51					1112.84

Sept 19, 1931
Cloudy 70°
P. Parks, T. Snyder

~~138~~
132.

N.W. root 15" Maple 50' Rt. sta. 48+30

8.12	5.09	C 3.0 / 25.0	6.93	C 1.2 / 23.0
7.97				

X S.W. cor. N. Parapet Culvert E.S. Chillicothe
Iron Bolt in Concrete, Intesection of ℄ Chillicothe
Road with ℄ of Cedar Road

7.93	5.56	C 2.4 / 23.0	7.20	C 0.7 / 21.0
11.18	10.02	C 1.2 / 22.0	10.08	C 1.1 / 22.0
14.18	15.45	F 1.3 / 19.0	15.06	F 0.9 / 17.0
9.18	9.18	0.0 / 9.0	9.18	0.0 / 13.5
8.59	7.39	C 1.2 / 21.5	7.49	C 1.1 / 21.0
6.34	4.51	C 1.8 / 23.0	6.11	C 0.2 / 22.0
5.84	4.41	C 1.4 / 22.5	5.50	C 0.3 / 21.0

N.E root 36" Beech 60' Rt. sta. 54+60

9.26	5.79	C 3.5 / 25.5	6.01	C 3.3 / 25.5
14.66	12.42	C 2.2 / 25.0	9.75	C 4.9 / 27.0
5.29	9.27	F 4.0 / 21.5	8.94	F 3.7 / 21.5
8.75	12.02	F 3.3 / 19.0	11.41	F 2.7 / 18.5

		1121.59									
50					1113.25	8,34	8,76	F0,4 19,5		9,48	F1,1 20,0
	11.73	1131.47	1.85	1119.74							
49					1117.55	13,92	8,16	C5,8 29,0		9,04	C4,9 26,0
48					1123,00	8,47	5,43	C3,0 25,0		7,25	C1,2 23,0
			10.15	1121,32							
B.M.				1121.30	Record	N.W. root 15" Maple 50' Rt. Sta. 48+30					

B.M.	7.79	1129.09		1121.30	
47+75					1123.15
47					1122.22
46					1120.67
45					1119.12
	2.87	1121.61	10.35	1118.74	
44					1117.57
43					1116.02
42					1114.47
41					1112.92
40					1111.60
	4.02	1116.15	9.48	1112.13	
39					1111.70
39+00	15" pipe culvert				
					1109.83
					1108.88
38					1113.24
	2.78	1118.35	0.58	1115.57	
37					1113.94
36					1112.50
35					1110.00

Sept. 21, 1931
clear 80°
D. Parks, T. Snyder

N. W. root 15" Maple 50' Rt, Sta. 48+30

5.94	2.87	C3.1 / 25.5		4.70	C1.2 / 23.0
6.87	4.93	C1.9 / 24.0		5.17	C1.7 / 22.5
8.42	9.19	F0.8 / 19.5		9.62	F1.2 / 19.5
9.97	9.89	C0.1 / 21.0		10.44	F0.5 / 21.0
4.04	3.41	C0.6 / 21.0		3.69	C0.4 / 20.5
5.59	6.64	F1.1 / 19.0		6.76	F1.2 / 19.0
7.14	6.75	C0.4 / 21.0		6.05	C1.1 / 22.0
8.69	8.47	C0.2 / 21.0		8.30	C0.4 / 21.5
10.01	10.14	F0.1 / 20.0		10.27	F0.3 / 20.0
4.45	6.14	F1.7 / 17.0		5.80	F1.4 / 17.5
6.32	5.32	C1.0'	stake 30' Lt.		1116.15 − 0.32 = 1110.83
7.27	4.27	C3.0'	stake 30' Rt.		
2.91	3.20	F0.3 / 20.0		3.34	F0.4 / 20.0
4.41	1.91	C2.5 / 23.0		2.73	C1.7 / 24.0
5.85	3.36	C2.5 / 24.5		3.89	C2.0 / 23.0
8.35	7.43	C0.9 / 21.5		7.15	C1.2 / 22.5

		1118.35			
34					1107.50
	4.20	1110.25	12.30	1106.05	
33					1106.00
32					1106.00
31					1106.00
30					1106.00
29					1106.00
28					1105.50
			2.93	1107.32	
B. M.	1.98	1109.23		1107.25	record
27+30					1104.55
27					1104.00
26					1102.00
25					1100.00
T. P			9.93	1099.30	

		F0.2		F0.4
10.85	11.05	20.5	11.26	20.5
		F1.7		F0.9
4.25	5.94	19.5	5.17	20.0
		F1.1		F1.3
4.25	5.39	19.0	5.51	19.5
		F1.6		F1.7
4.25	5.88	19.5	5.95	19.0
		F0.3		C0.2
4.25	4.57	20.5	4.01	21.0
		F0.6		C0.1
4.25	4.85	20.0	4.15	20.5
		F0.7		C0.1
4.75	5.47	20.0	4.61	21.5
R.R spike S.W. side Dead Elm 33.5' Lt, sta 27+30				
		C2.3		C2.2
4.68	2.38	24.0	2.53	24.0
		C2.3		C1.8
5.23	2.92	23.0	3.48	23.0
		F0.5		0.0
7.23	7.75	19.0	7.21	20.5
		F0.7		F1.7
9.23	9.93	19.5	10.90	17.0
Slope Hub Lt, sta. 25+00				

T.P.	2.04	1101.34		1099.30	
24					1098.00
23					1096.00
22					1093.75
21					1091.00
	6.05	1094.55	12.84	1088.50	
20					1088.00
19+50					1086.50
19					1085.00
	1.88	1084.70	11.73	1082.82	
18					1082.00
17					1079.75
16					1079.00
15					1078.00
	9.95	1090.24	4.41	1080.29	
14					1079.63
13					1084.44
			2.72	1087.52	
B.M.	10.53	1098.05		1087.52	record
12					1092.50
	11.35	1108.93	0.47	1097.58	
11					1101.00
	11.34	1119.13	1.14	1107.79	
10					1109.50
	12.56	1129.16	2.53	1116.60	
9					1118.00
T.P.			0.49	1128.67	

Sept, 22, 1931
D. Parks cloudy
T. Snyde Windy } 80°

Slope Hub Lt. sta. 25+00

		0.0		F0.1
3.34	3.32	21.5	3.47	20.5
		F0.6		C1.4
5.34	5.97	18.0	3.95	22.5
		F1.4		0.0
7.59	9.00	17.0	7.61	20.5
		C0.3		C1.5
10.34	10.80	20.0	8.87	22.5
		F0.4		C5.9
6.55	6.93	20.0	0.66	27.5
		F1.7		C5.6
8.05	9.70	19.5	2.50	28.0
		F2.2		C2.8
9.55	11.75	19.5	6.72	24.5
		F1.3		C0.8
2.70	4.02	19.0	1.88	21.5
		F0.9		F1.3
4.95	5.83	17.0	6.27	20.0
		F1.0		F1.3
5.70	6.68	17.0	7.00	20.0
		F0.3		F1.7
5.70	6.04	17.0	7.35	18.5
		C0.7		F1.7
10.61	9.91	18.5	12.04	17.0
		F1.3		F4.8
5.80	7.13	17.0	10.57	22.5

Spike S. root 20" Maple 45' Lt. sta. 12+72

		F4.2		F1.1
5.55	9.79	23.0	6.61	20.5
		F3.3		C0.6
7.93	11.24	25.0	7.32	18.0
		F2.1		C1.1
9.63	11.70	25.0	8.55	17.0
		C4.8		C0.5
11.16	6.37	24.0	10.64	16.0

Slope Hub Rt. sta. 8+00

0+18 15" pipe Culvert

B.M.	4.21	1148.89	1144.68

Sept, 22, 1931
D. Parks
J. Snyder

R.P. iron pipe 43.10' N.W. of intersection of center Line of N. & S. road with Center line of E. & W. road

1139.75	8.94	4.94	C 4'0" stake 30' Rt
1149.25	4.64	1.64	C 3'0" stake 30' Lt

	12.07	1140.74		1128.67	
8					1126.50
7	13.06	1153.76	0.04	1140.70	1135.00
6					1144.00
5+50					1148.88
5	12.23	1163.70	2.29	1151.47	1154.00
B.M.			13.70	1150.00	
4+50				1150.12	record
B.M.			4.20	1159.50	1159.25
				1159.60	record
B.M.	10.62	1155.30		1144.68	record
0+50					1148.75
1 00	13.00	1167.75	0.55	1154.75	1154.00
1+50	10.75	1177.05	1.45	1166.30	1159.25
2					1164.50
3	4.33	1180.17	1.21	1175.84	1169.75
4	1.89	1169.75	12.31	1167.86	1164.50
B.M.			10.20	1159.55	
4+50				1159.60	record
					1159.25

Sept. 23, 1931
D. Parks cloudy 80°
T. Snyder

Slope Hub Rt. Sta. 8+00

14.24	7.56	C6.7 / 26.0	12.07	C2.1 / 17.0
5.74	3.75	C2.0 / 23.0	6.30	F0.6 / 16.0
9.76	10.60	F0.9 / 21.0	12.73	F3.0 / 19.0
4.88	5.57	F0.7 / 21.0	9.43	F4.6 / 22.0
9.70	10.44	F0.8 / 20.5	12.23	F2.7 / 19.0

Spike Bent so that B.M. is ruined spike also loosened

Spike N. side 20" Apple Rt. Sta. 5+00

Iron Pipe looks to have been Hit

R.P. 25+00 iron pipe Rt. sta. 4+45

R.P. 43.10 iron pipe

6.55	3.90	C2.7 / 20.0	5.95	C0.6 / 19.0
13.75	6.31	C7.4 / 25.0	10.75	C3.0 / 20.0
17.80	9.31	C8.5 / 27.0	14.61	C3.2 / 23.0
12.55	4.98	C7.6 / 27.5	9.51	C3.0 / 19.0
10.42	2.60	C7.8 / 25.0	7.91	C2.5 / 21.0
5.25	+0.35	C5.6 / 22.0	4.53	C0.7 / 23.0

R.P. iron pipe Rt. sta. 4+45

10.50	4.92	C5.6 / 25.0	11.33	F0.8 / 21.0

		1169.75				
	0.60	1159.00	11.35	1158.40		
5					1154.00	
			8.93	1150.07		
B. M.	8.93	1159.05		1150.12	record	

Spike N. side 20" Apple Rt. sta. 5+00
Spike is Bent down and loosened from tree

sept. 28, 1931
Fair 70°
P. Parks T. Snyder

40+00	15" pipe Culvert					
Culvert Stake						
Left 39+00	14.61	1115.44		1110.83		
					1109.83	5.61
					1108.88	6.56

2.61 cut 3'0" Stake 30' Lt.
3.56 cut 3'0" Stake 30' Rt.

FZ.5
7.51 19.0

147

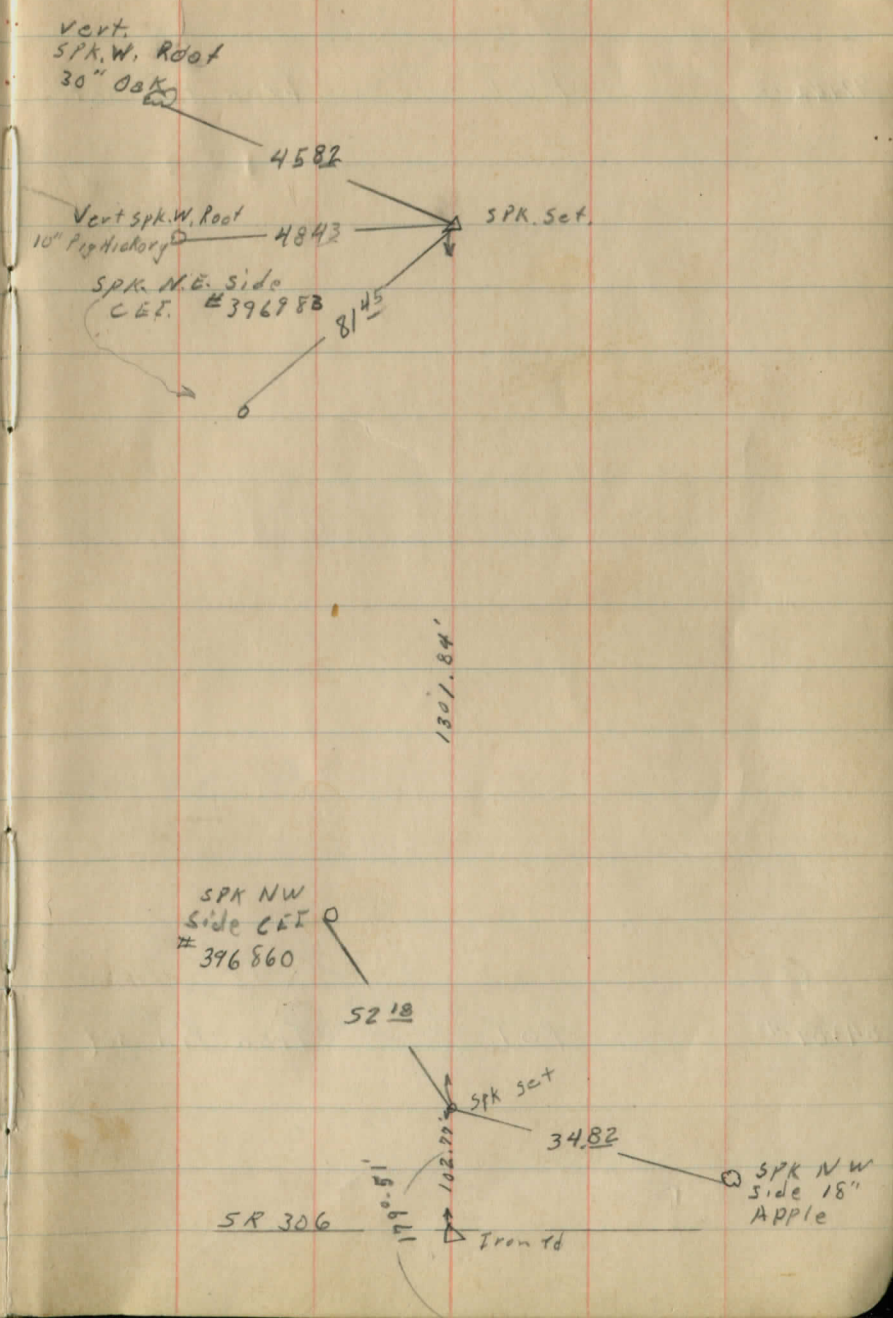
Ceder Road sec "C"

H. Patterson
P. Young
B. Moss

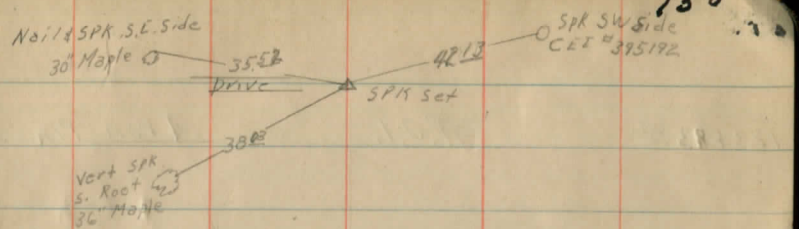
8-2-60 Cloudy - windy - Hot 85°

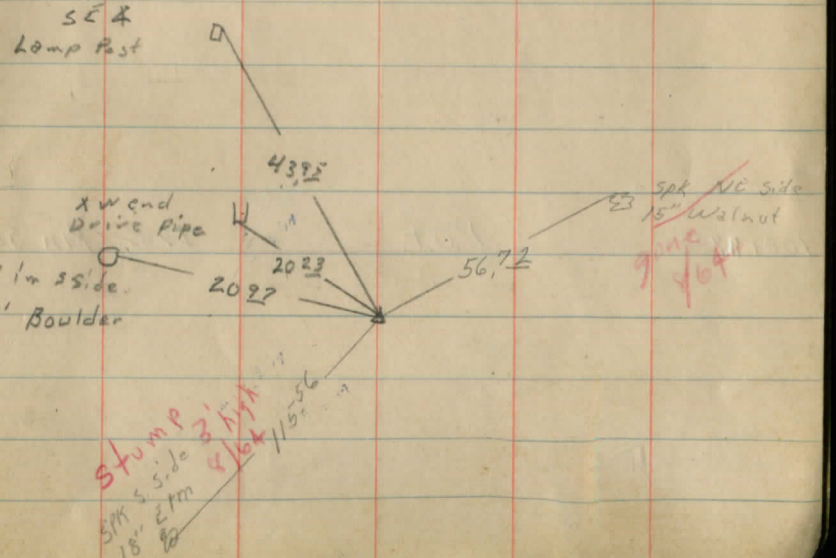
76+40.61	P.O.t.	Iron Pin set
63+38.77	P.O.t.	Iron Pin set
62+36		

148



97+42.62	P.O.T.	Iron Pin set
84+89.48	P.O.T.	Iron Pin set

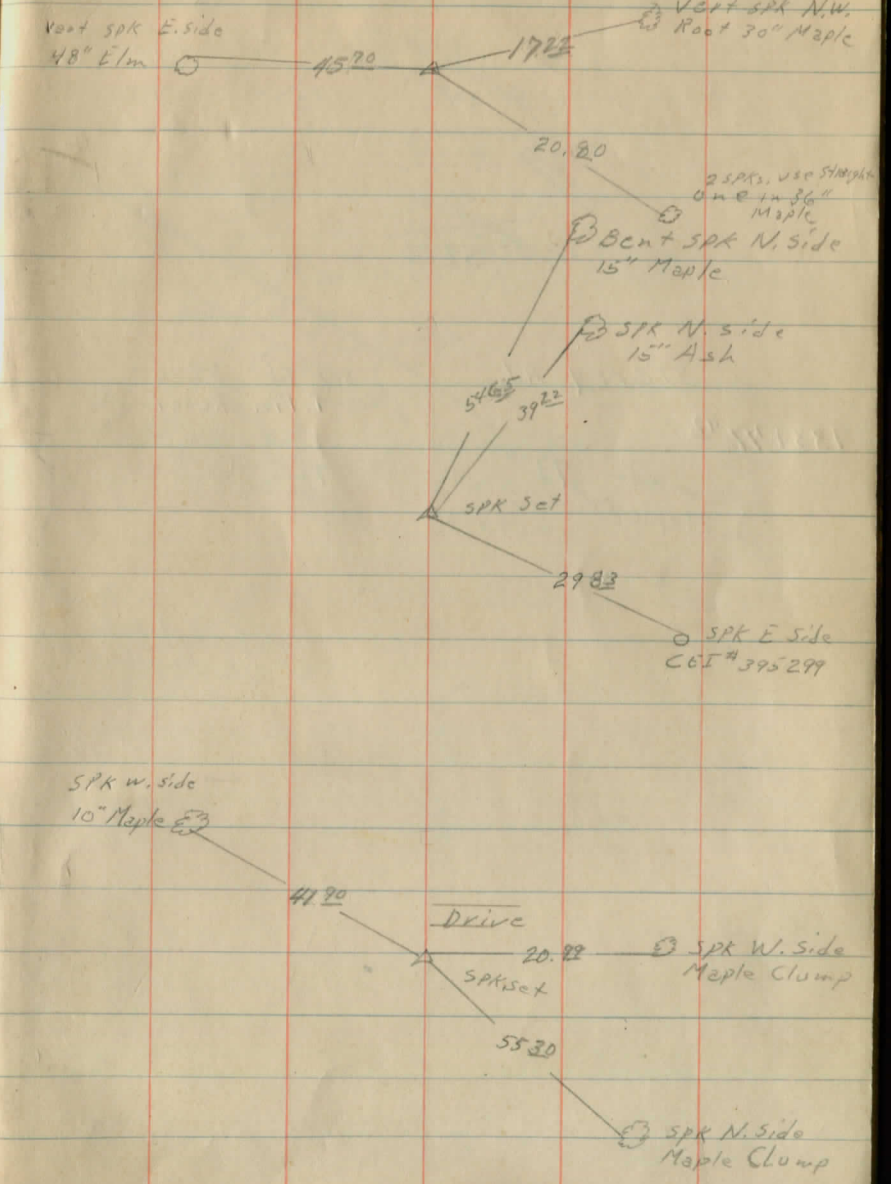




123+93.62 P.O.T. Iron Pin Set

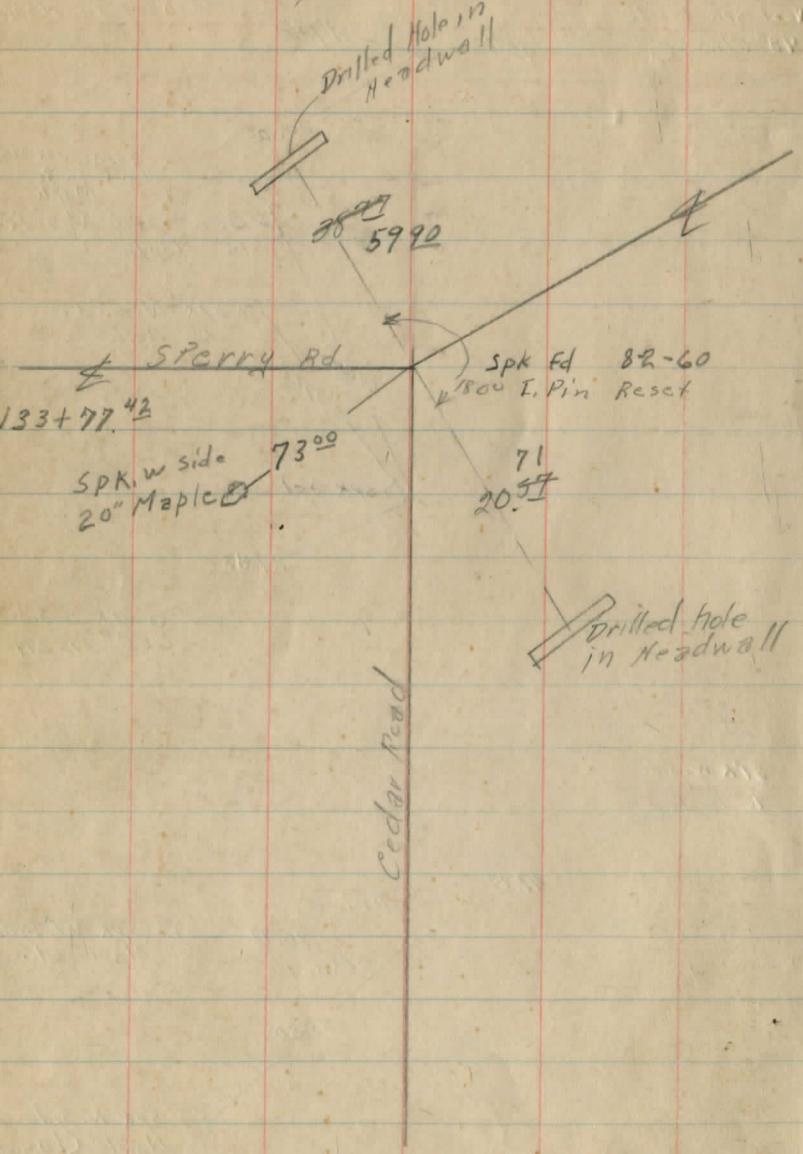
116+54.72 P.O.T. Iron Pin Set

108+99.30 P.O.T. Iron Pin Set



153

References by Krause Mar 28, 1936



215.10

150)1189
1150
81.39
81.50
18.80
8768.80
2923
8798.23
2178

179 - 51 1
359 - 42 2
179 51
539 - 33
360
179 - 33 3

1361.84
102.77
1464.61

16.87
26
17.22
17.01

4610
46
4564.20

20.08
.22

Table IX.—Calculation of Earthwork.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if w =16.2 and h =5.3, cu. yds. =1.48+.028+.089 =1.597 cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) =h, and ½ the roadbed =w, add the triangles formed by taking the distance out to each break in turn (=w's) by the difference between the cuts (or fills) on each side of it (=h's) always subtracting the outer from the inner.

Distances from Center of Roadway for Cross-Sectioning.

Roadway 16 feet wide. Side Slopes 1 on 1½.

For Single Track Embankments.

0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.0	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54 2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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